



*Unité Sciences du Bois et des Biopolymères*

*Université Bordeaux 1 /CNRS/INRA*

*Modelling load duration of  
timber beams under  
various relative humidity conditions*

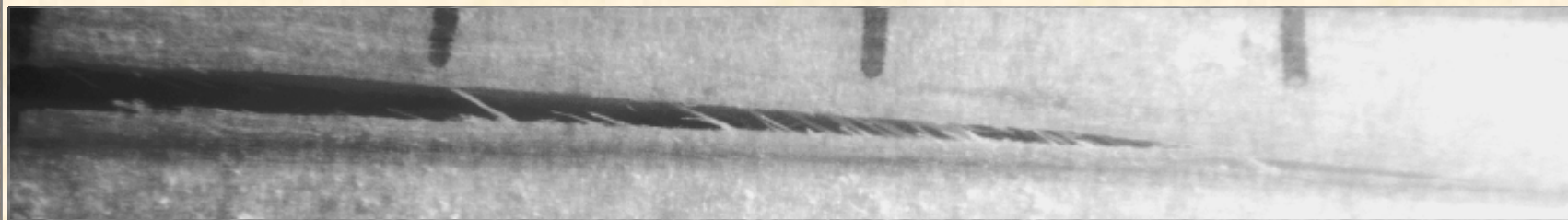
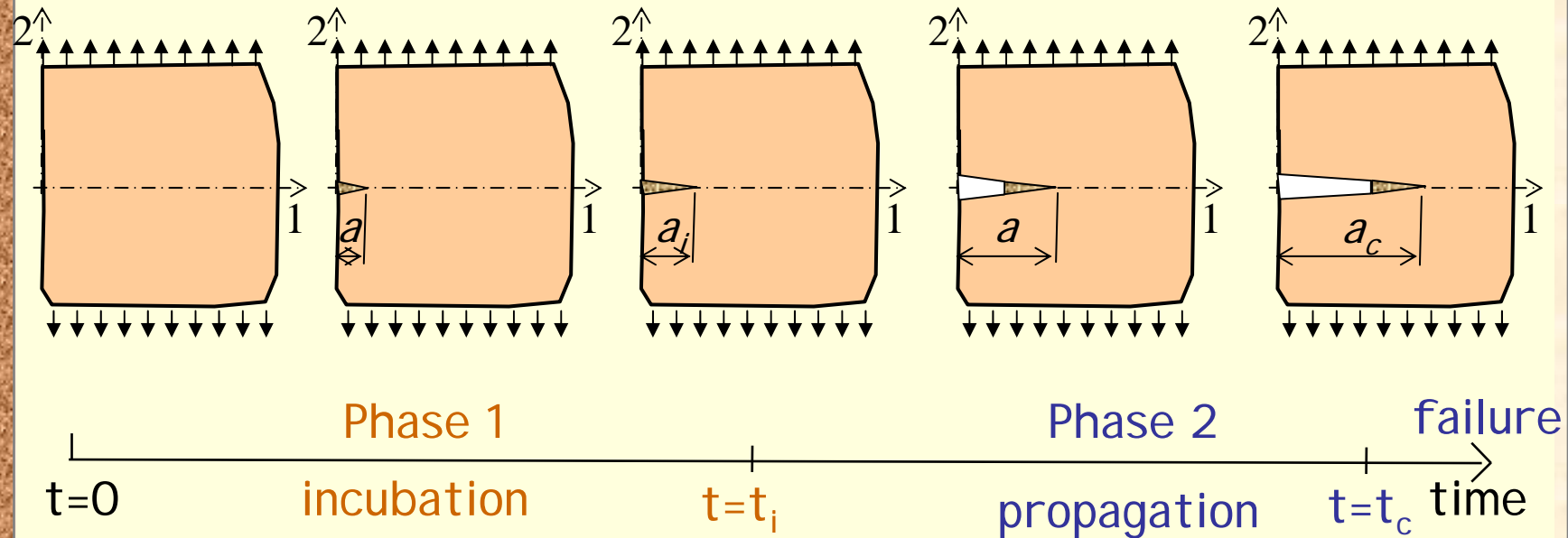
*Myriam CHAPLAIN*

*Modelling of the Performance of Timber Structures Eindhoven oct.2007*

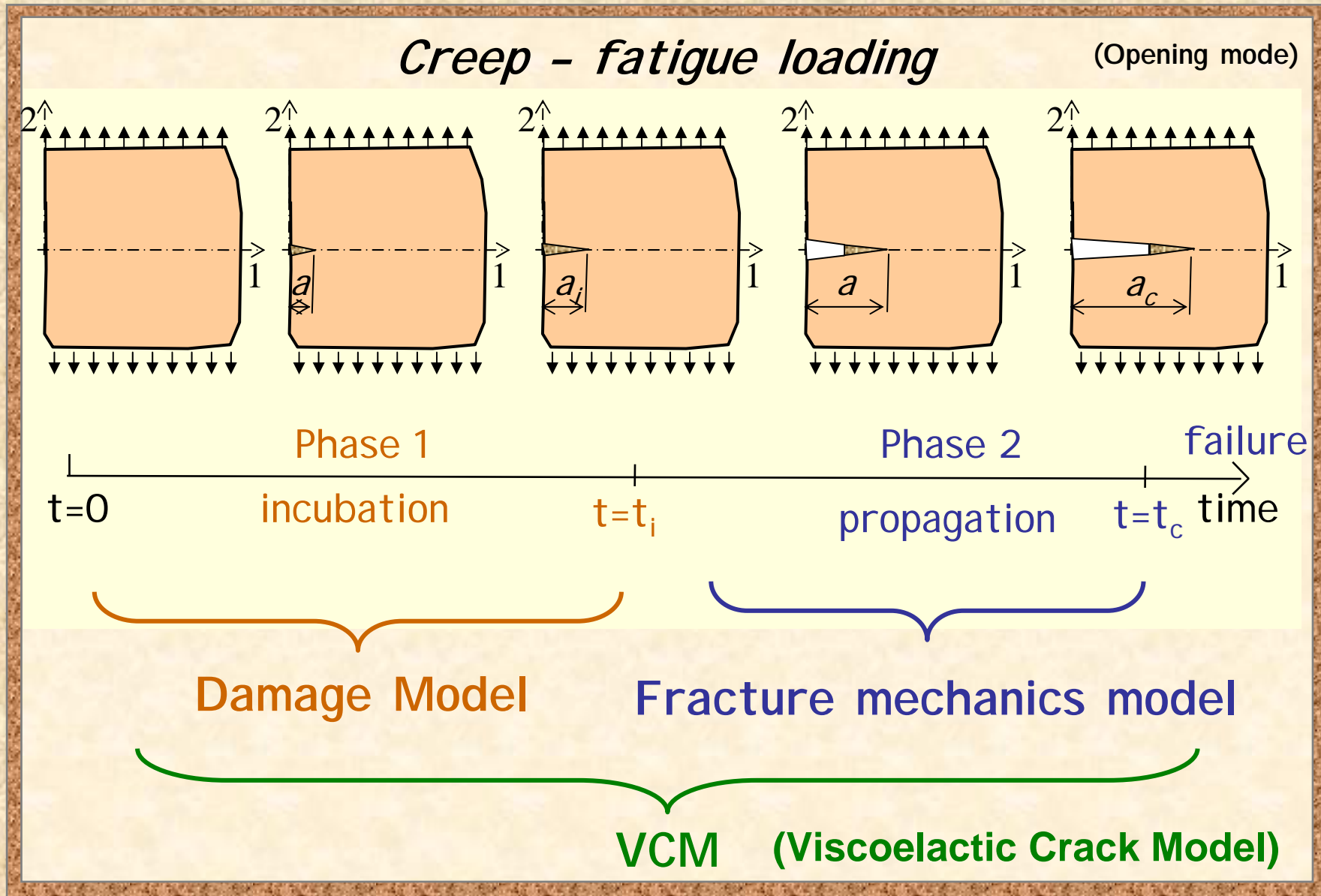
# Introduction

## Creep - fatigue loading

(Opening mode)



# Introduction



- ➡ **Experimental observations**
- ➡ **Viscoelastic Crack Model (VCM)**
- ➡ **Predictions / experiments**
- ➡ **Conclusion /objectives**

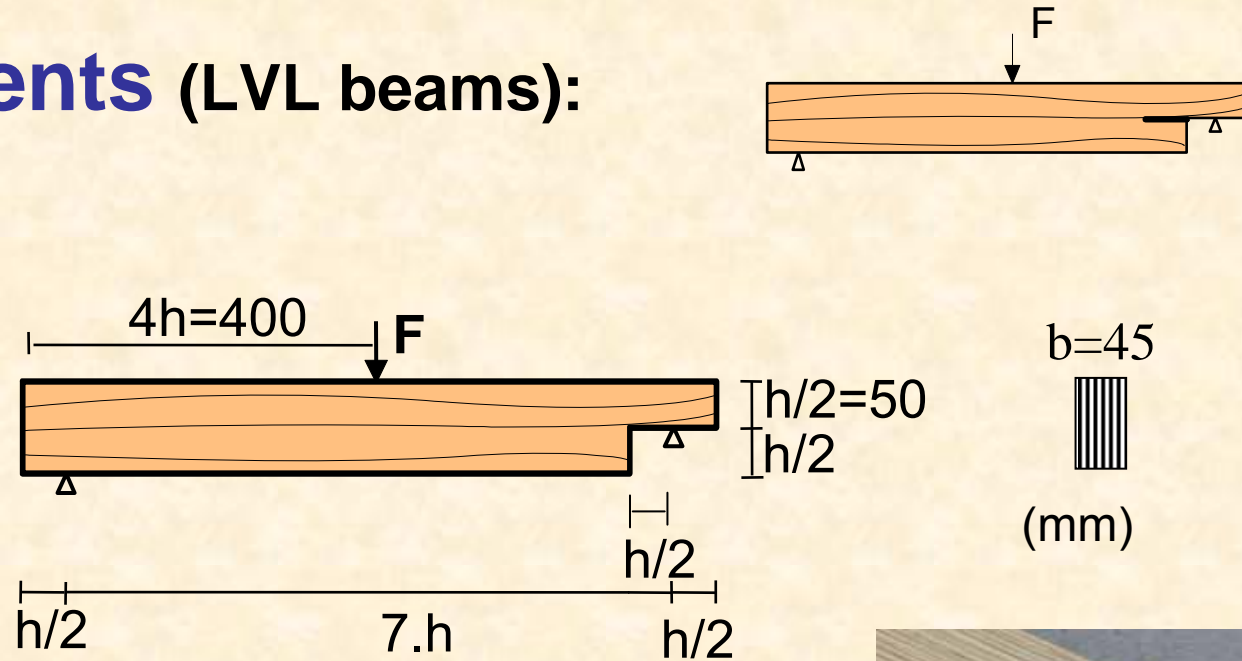
**EXPERIMENTAL**

**OBSERVATIONS**

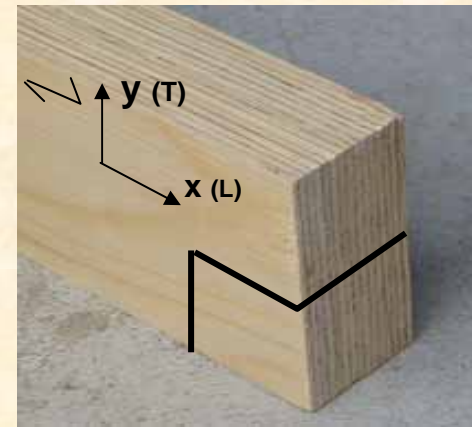


# Experimental observations

## Experiments (LVL beams):



Inside - Outside



# Experimental observations

## Experiments (LVL beams):

### ✓ Short term tests

- Strength ( $F_s$ )  $\Rightarrow$  Stress Level SL

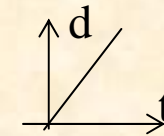
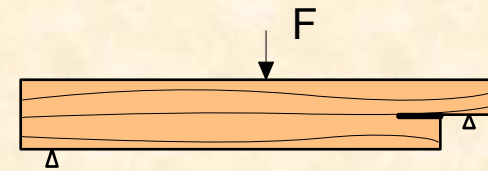
$$SL = F / F_s$$

### ✓ Long term tests

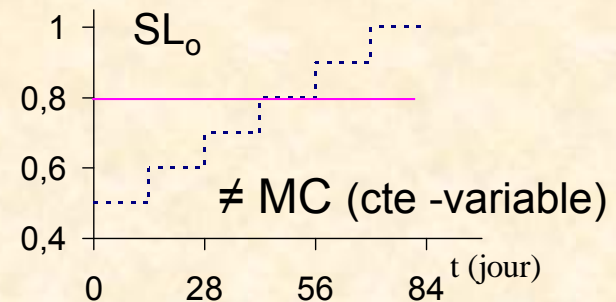
- Incubation time ( $t_i$ )
- Propagation time ( $t_p$ )

$$F = SL_0 \cdot F_{s0}$$

### ↪ Time to failure ( $t_r$ )

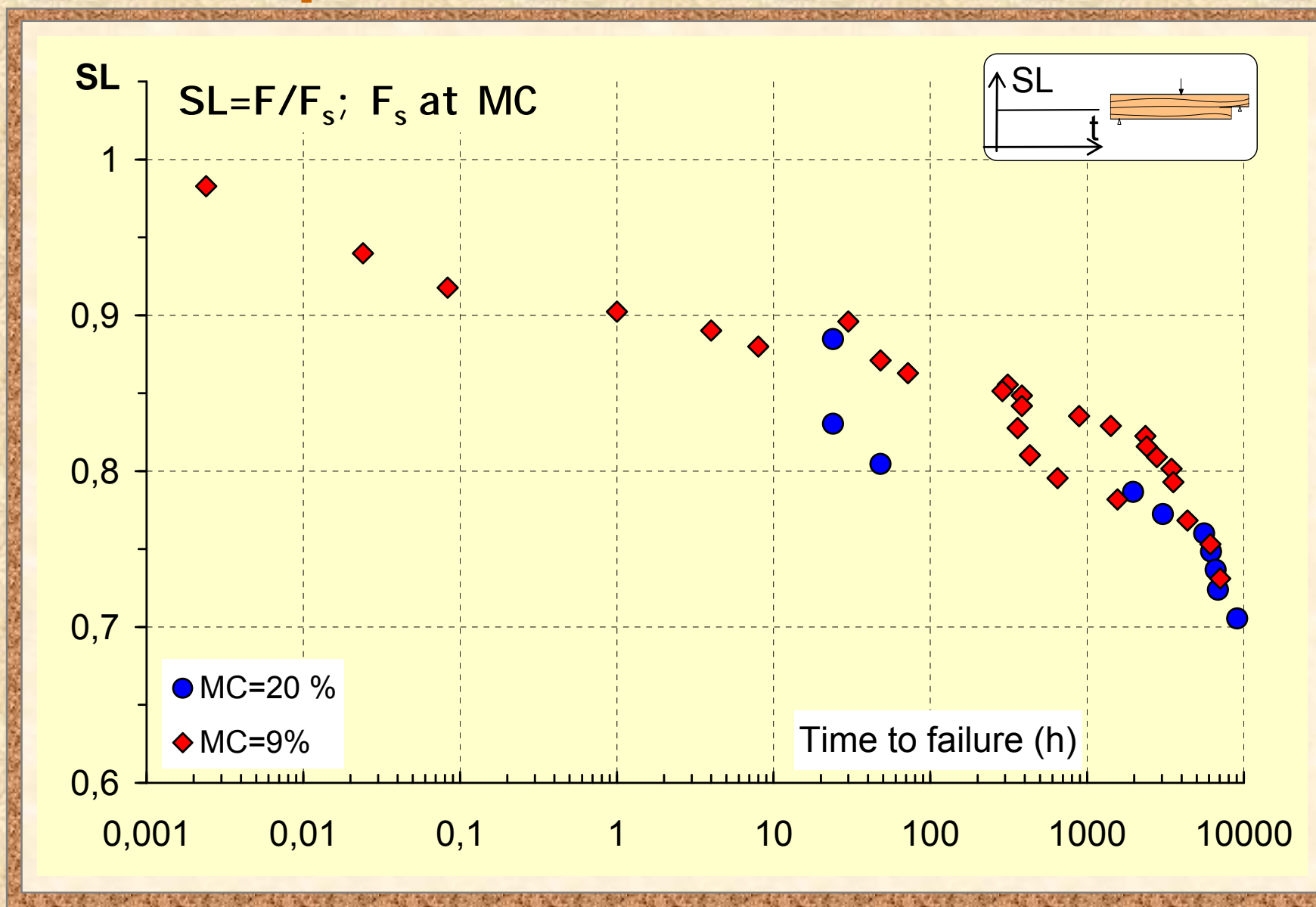


$\neq$  MC (9% - 20%)



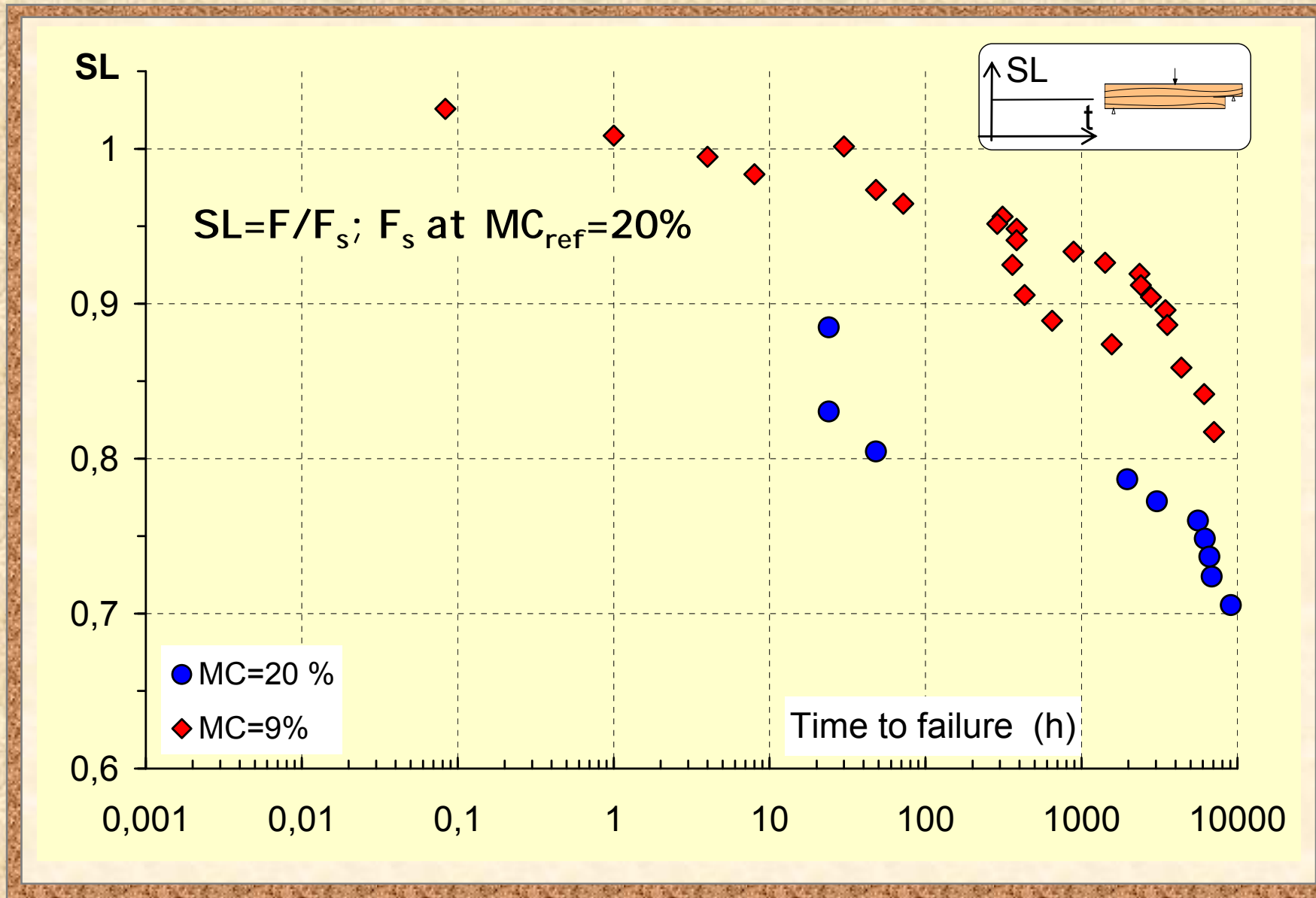
$F_{s0}$  = average strength (MC=20%)

# Experimental observations

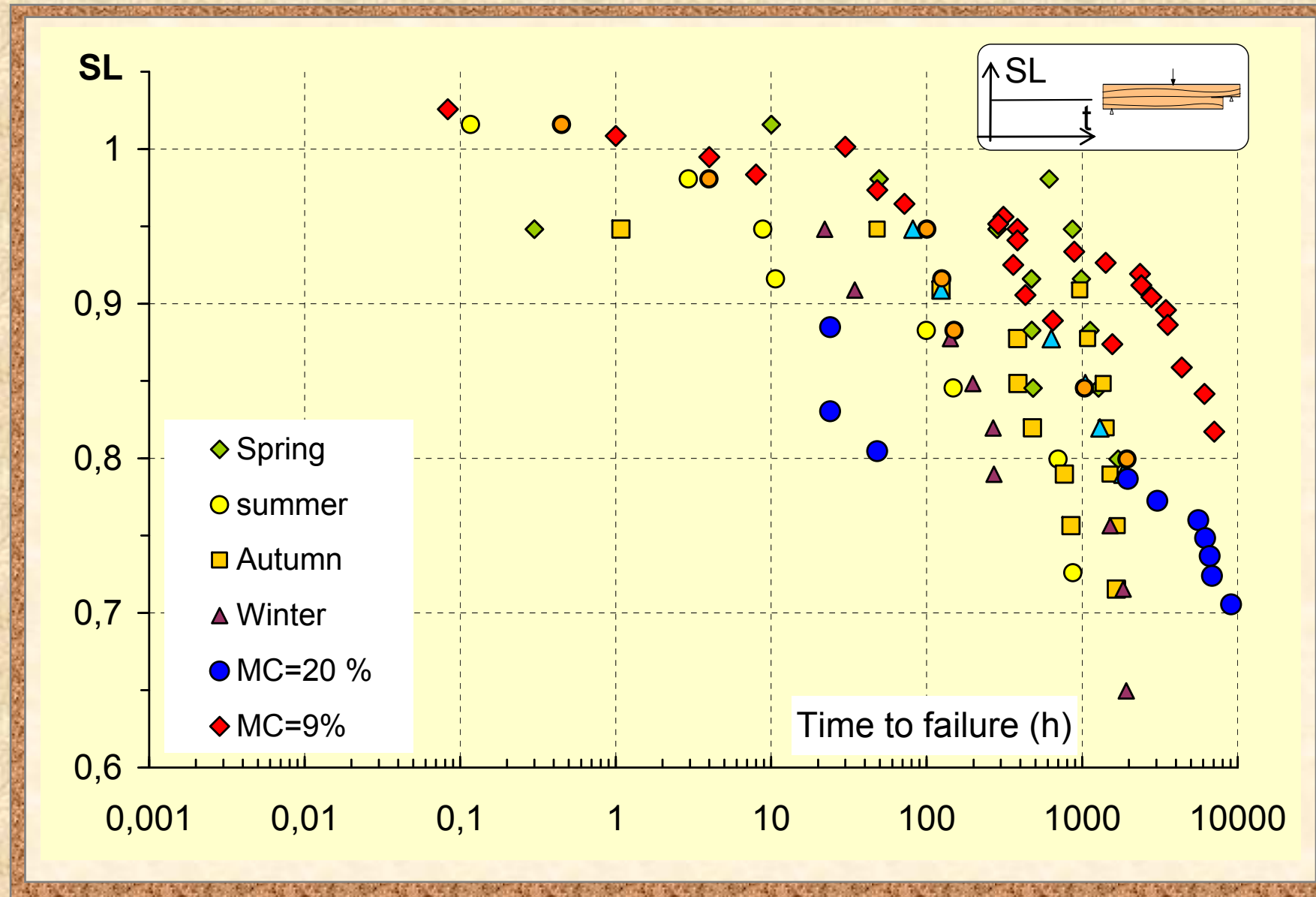




# Experimental observations



# Experimental observations



# Experimental observations

For a given  $SL = F/F_s$  with  $F_s$  at  $MC_{ref} = 20\%$  :

☞ **Time to failure**                      **dry  $\geq$  wet**

☞ **Incubation time**                      **dry  $<$  wet**

☞ **Propagation time**                      **dry  $>$  wet**

# Viscoelastic Crack Model

# Incubation – Damage modelling

## Damage model

$$\left\{ \begin{array}{l} \frac{dD}{dt} = a \cdot \left( \frac{F}{F_s} - \frac{F_o}{F_s} \right)^b + c \cdot D \quad \text{if } F > F_o \\ \frac{dD}{dt} = 0 \quad \text{if } F \leq F_o \end{array} \right.$$



$F_s$  :  $F_s$  at  $MC_{ref}=20\%$

( $D$  : damage parameter)

✓  $t=0 \quad D=0 \Rightarrow t=t_i \quad D=D_i$

Notched LVL beam with a process zone = 5 mm

$a_i = 5 \text{ mm} \quad \Rightarrow \quad D_i \approx 0,01 \quad (\text{Cast3M})$

✓  $F_o/F_s = SL_o$  : function of MC

$SL_o = 0,55$  for  $MC=9\%$

$SL_o = 0,60$  for  $MC=20\%$



# Crack propagation modelling

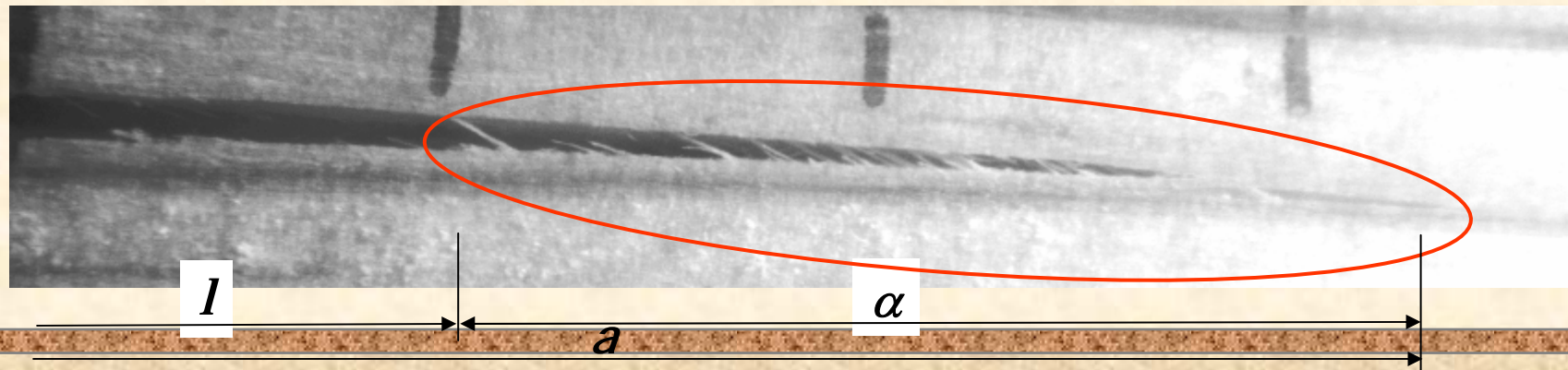
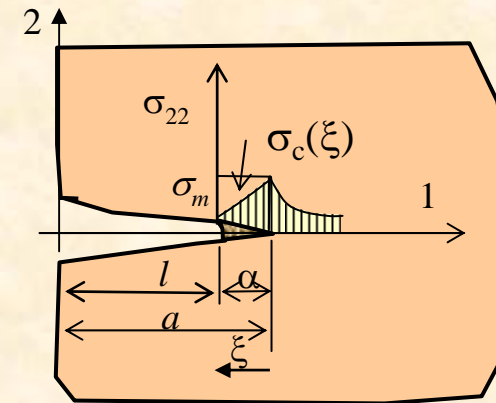
**Propagation**

$$\frac{da}{dt} = \frac{\pi}{2} \left[ \frac{C_2 \lambda_n}{(K_{Ic}^2 - K_I^2)} \right]^{\frac{1}{n}} \frac{K_I^{2(1+\frac{1}{n})}}{(\sigma_m I_1)^2}$$

☞  $\sigma_m, I_1$  (function of MC)

$$\sigma_m = \text{Max}_{0 < \xi < \alpha} (\sigma_c(x))$$

$$I_1 = \int_0^\alpha \left[ \frac{\sigma_c(\xi)}{\sigma_m} \frac{1}{\sqrt{\alpha \cdot \xi}} \right] d\xi$$



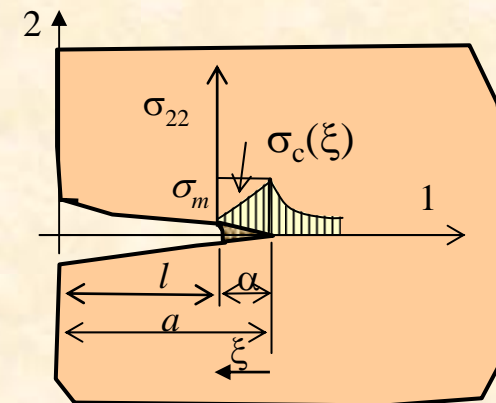
# Crack propagation modelling

**Propagation**

$$\frac{da}{dt} = \frac{\pi}{2} \left[ \frac{C_2 \lambda_n}{(K_{Ic}^2 - K_I^2)} \right]^{\frac{1}{n}} \frac{K_I^{2(1+\frac{1}{n})}}{(\sigma_m I_1)^2}$$

☞  $\sigma_m, I_1$  (function of MC)

$$\sigma_m = \text{Max}_{0 < \xi < \alpha} (\sigma_c(x)) \quad I_1 = \int_0^\alpha \left[ \frac{\sigma_c(\xi)}{\sigma_m} \frac{1}{\sqrt{\alpha \cdot \xi}} \right] d\xi$$



☞ **Reduced compliance**  $\kappa^v(t) = C_0(1 + C_2 t^n)$  (function of MC)

↻  $\lambda_n = 3\sqrt{\pi}\Gamma(n+1)/[4(n+3/2)\Gamma(n+3/2)]$  avec  $\Gamma(n) = \int_0^\infty t^{n-1} e^{-t} dt$  (function gamma)

# Crack propagation modelling

**Propagation**

$$\frac{da}{dt} = \frac{\pi}{2} \left[ \frac{C_2 \lambda_n}{(K_{Ic}^2 - K_I^2)} \right]^{\frac{1}{n}} \frac{K_I^{2(1+\frac{1}{n})}}{(\sigma_m I_1)^2}$$



**Stress intensity factor**

$$K_I(a) = \frac{F}{b\sqrt{w}} g(a/w)$$

( $b$  : thickness -  $w$  : characteristic dimension of the specimen )

$g$  : calibration function depending on MC

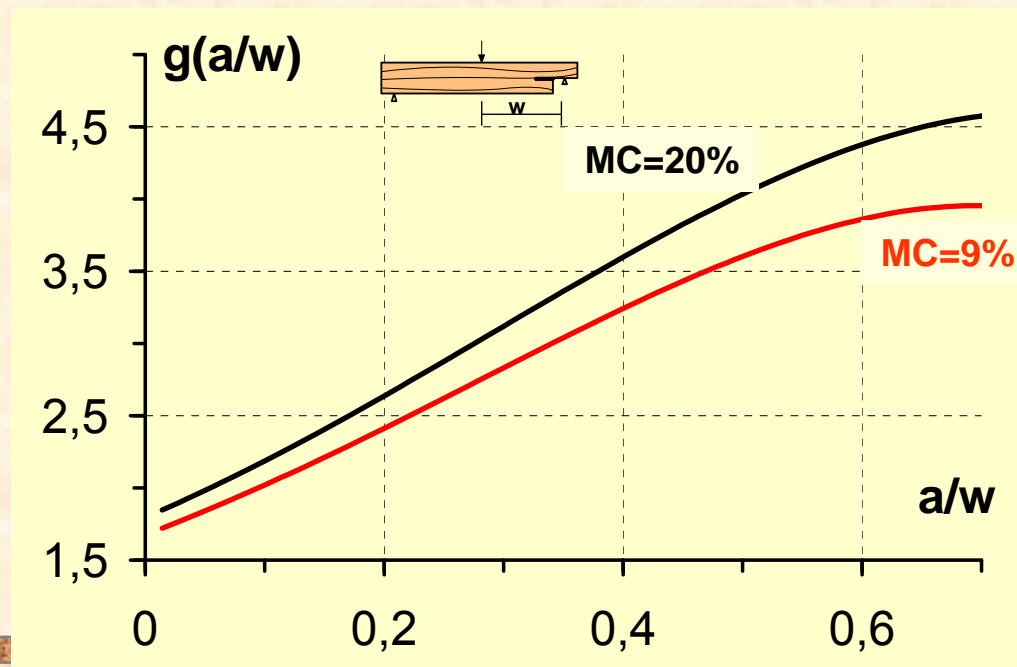
# Crack propagation modelling

Propagation

$$\frac{da}{dt} = \frac{\pi}{2} \left[ \frac{C_2 \lambda_n}{(K_{Ic}^2 - K_I^2)} \right]^{\frac{1}{n}} \frac{K_I^{2(1+\frac{1}{n})}}{(\sigma_m I_1)^2}$$

☞ Stress intensity factor

$$K_I(a) = \frac{F}{b\sqrt{w}} g(a/w)$$



# Crack propagation modelling

**Propagation**

$$\frac{da}{dt} = \frac{\pi}{2} \left[ \frac{C_2 \lambda_n}{(K_{Ic}^2 - K_I^2)} \right]^{\frac{1}{n}} \frac{K_I^{2(1+\frac{1}{n})}}{(\sigma_m I_1)^2}$$

 **Stress intensity factor**

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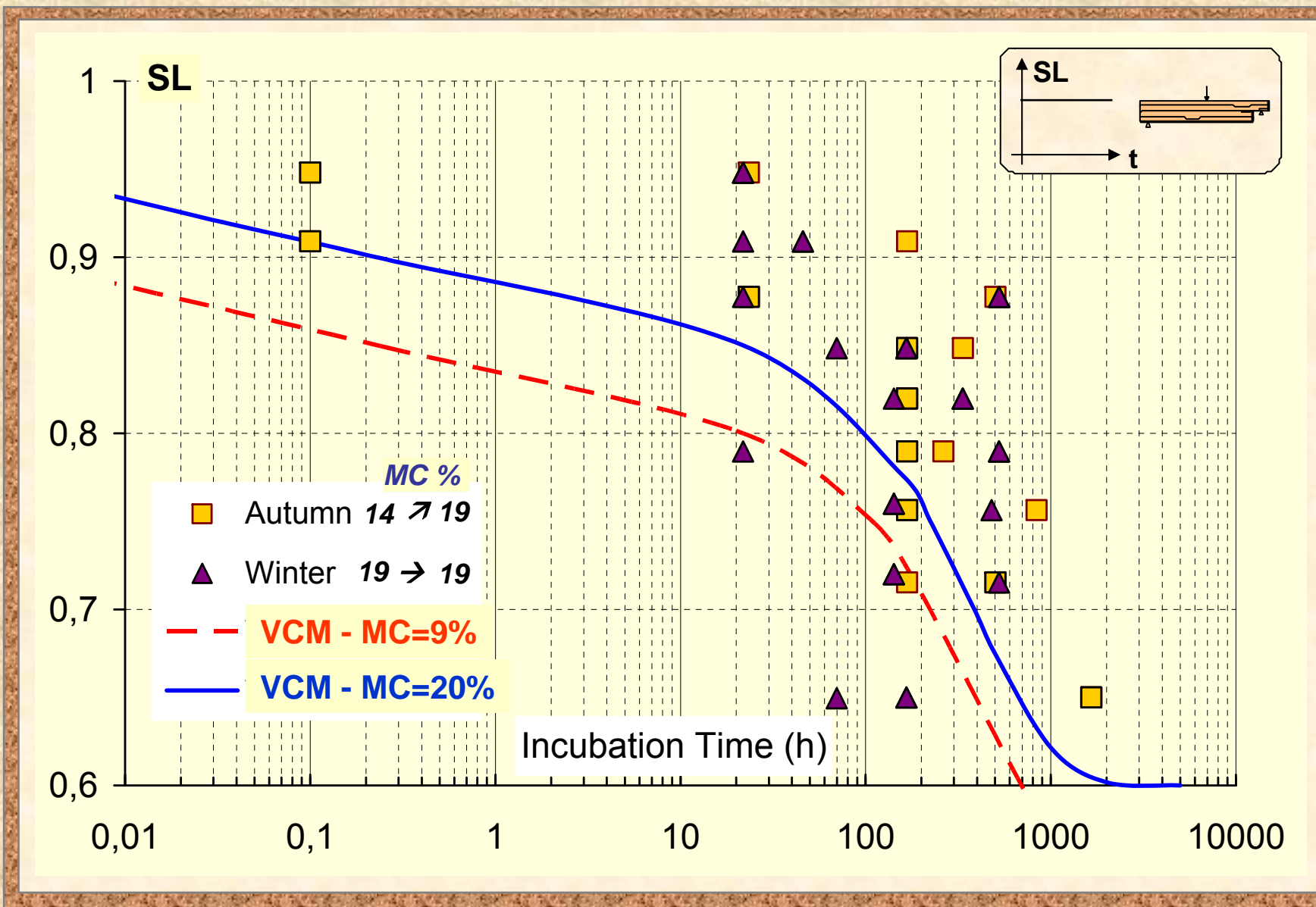
$$\text{Failure} \quad K_I = K_{Ic} = \sqrt{2G_I / C_o}$$

$G_I$  : Fracture energy (not depending on MC)

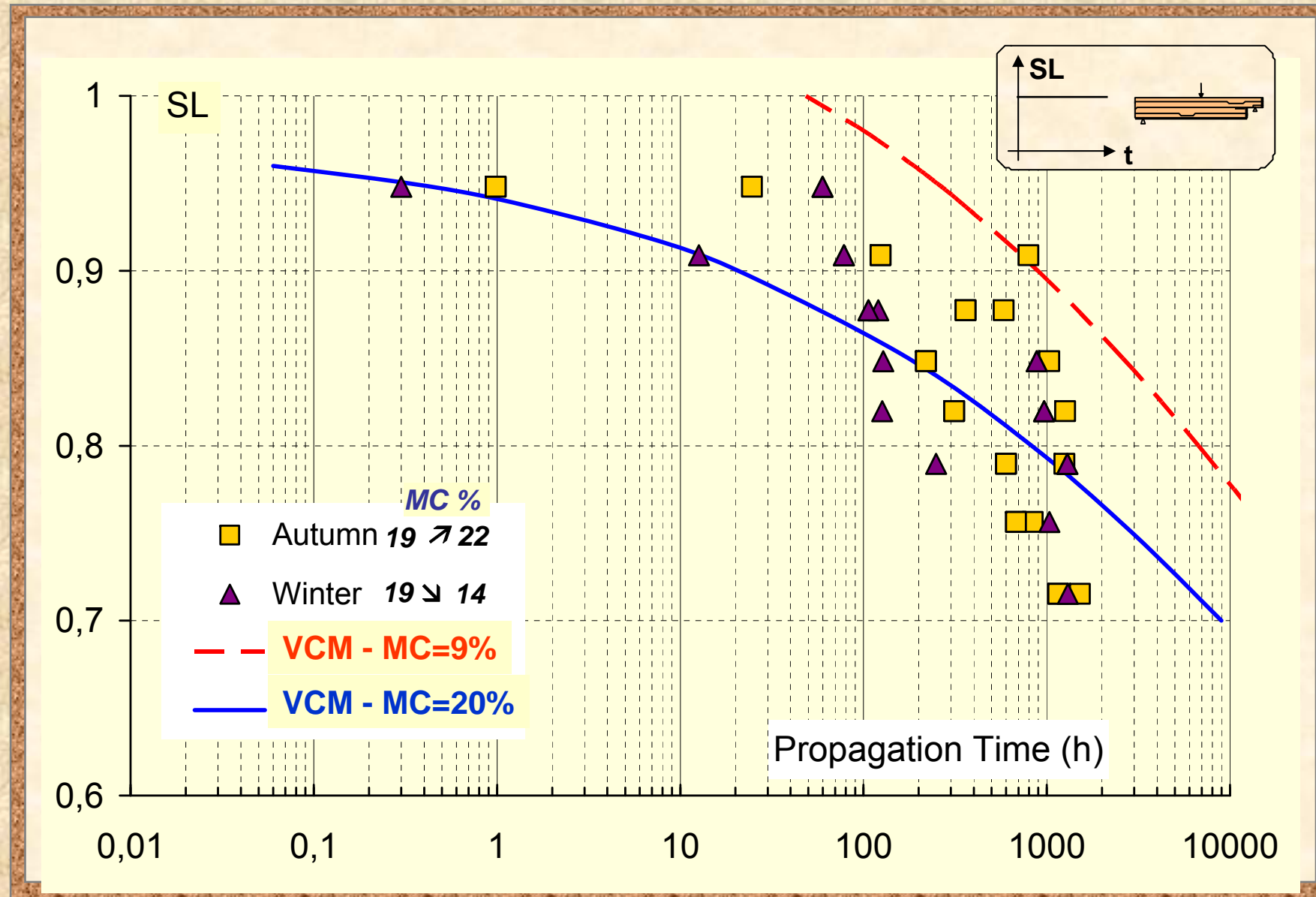


# Predictions vs experiments

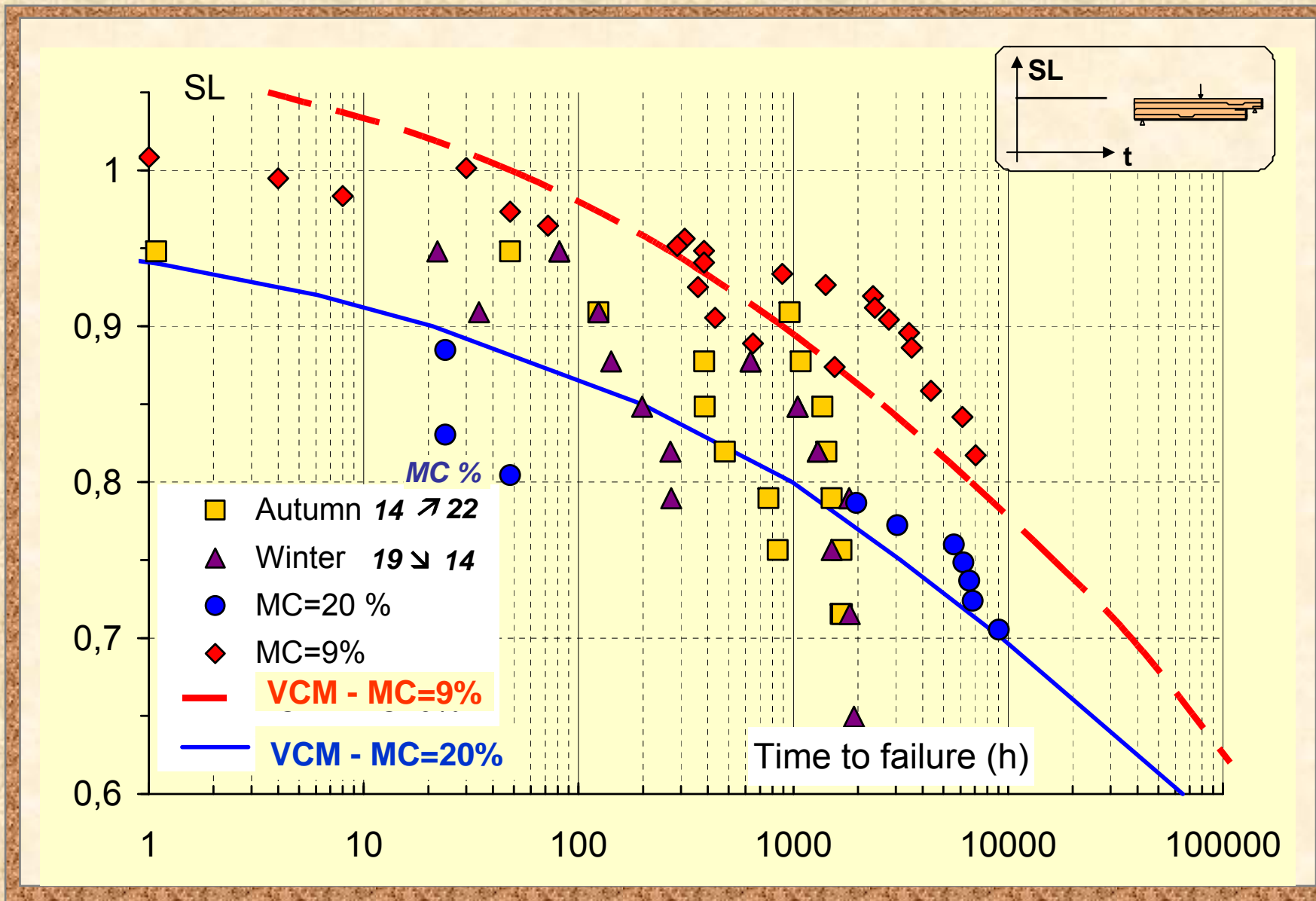
# Incubation time



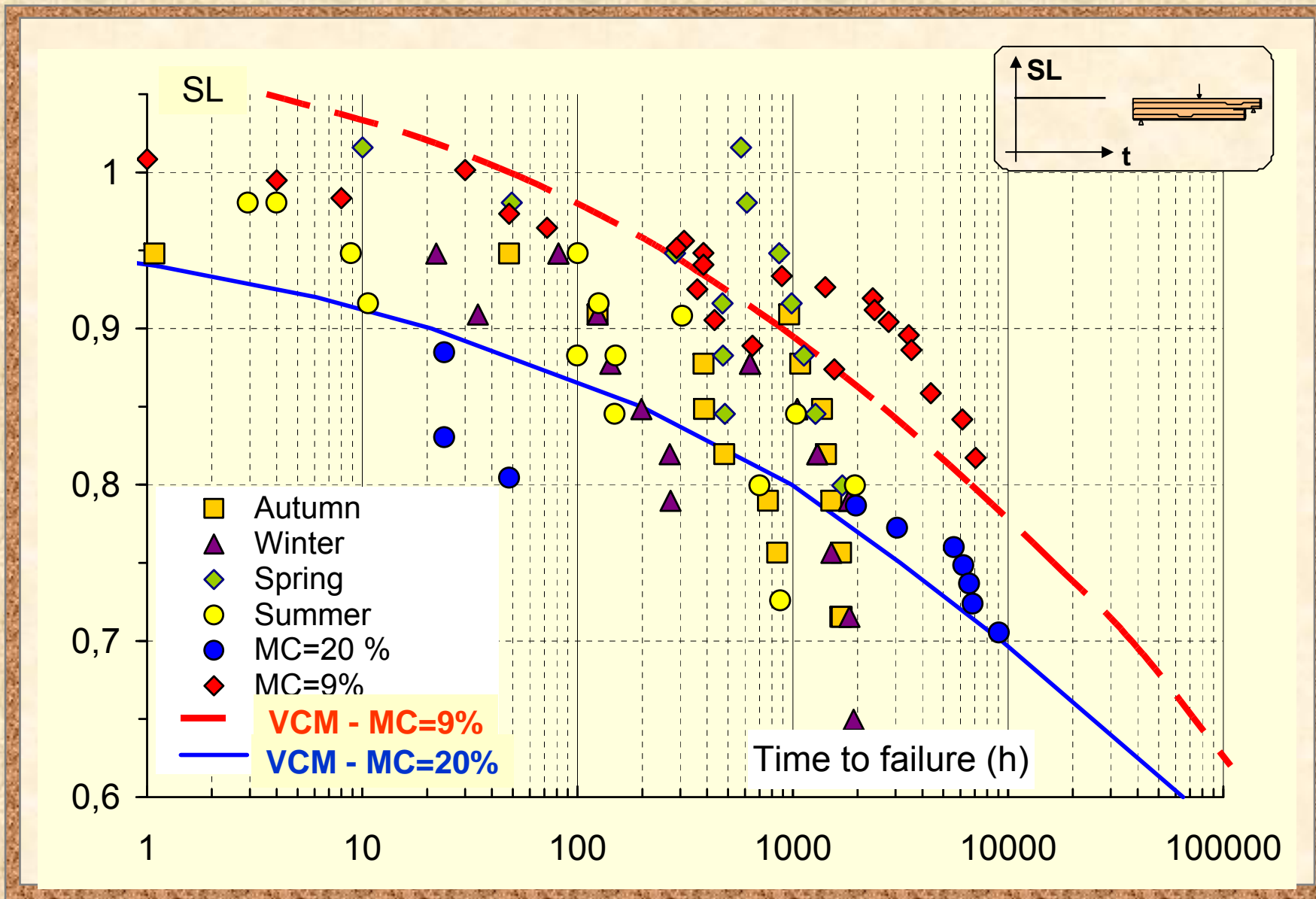
# Propagation time



# Time to failure



# Time to failure





# Conclusion

## ✓ Influence of relative humidity:

- ✎ Incubation time                      dry < wet
- ✎ Propagation time                      dry > wet
- ✎ Time to failure                        dry ≥ wet

(Scattering of experimental results)

## ✓ Delayed Fracture VCM:

- ✎ Incubation : damage model
  - ✎ Propagation : NLEF model
- } Time to failure

**Under stabilized MC**

# Objectives

- ✓ Introduce MC change effects into VCM
- ✓ Modelling climate scenarios  
(Probabilistic approach) :  $(HR, T^\circ) \rightarrow MC$

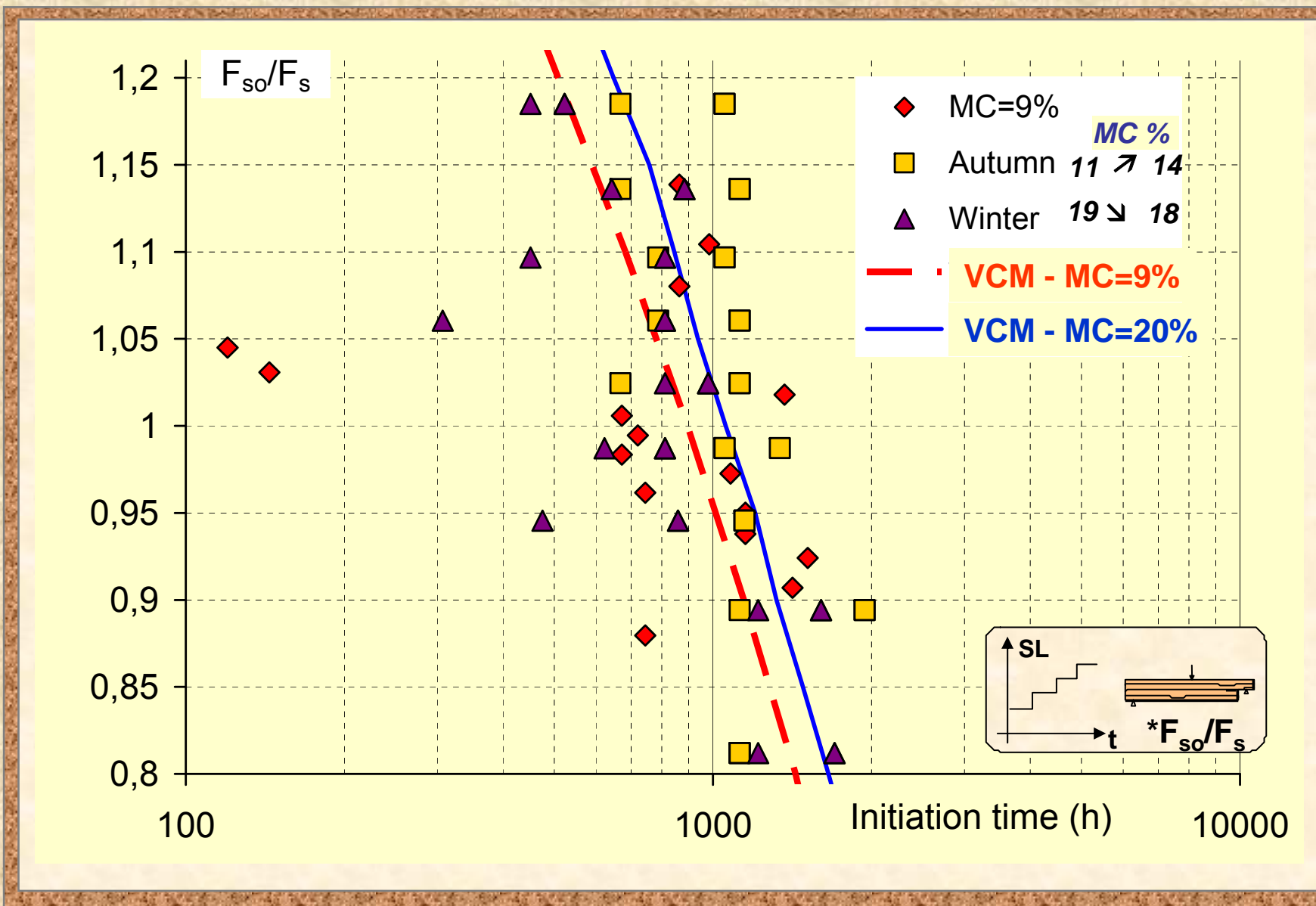
## Connection with the WG2 actions

☞ lifetime of timber structure elements

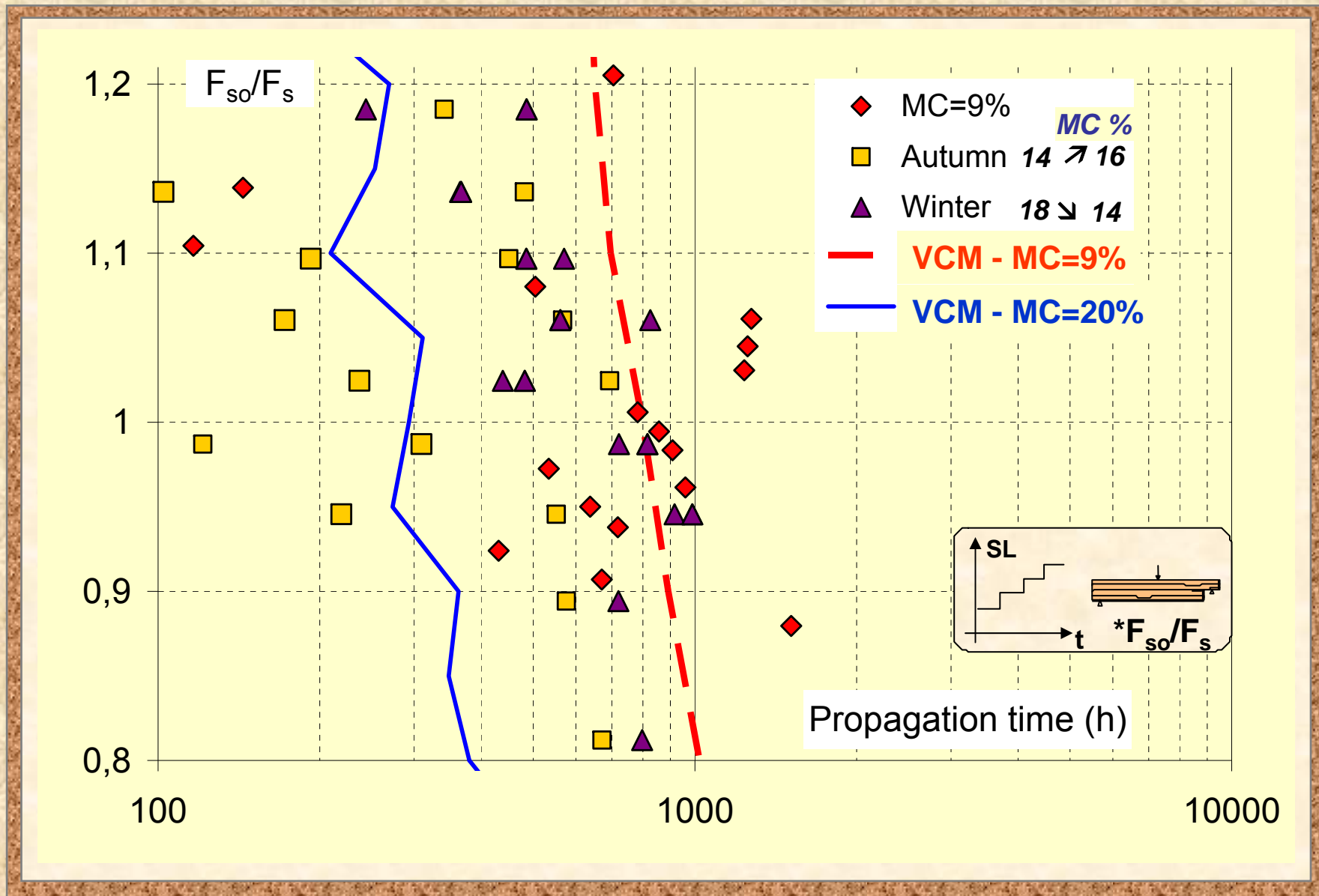
- ✓ "Dependency climate scenarios which might occur during the lifetime of the structure"
- ✓ "Modelling of moisture-related degradation and service-life assessment of timber components"

THE END

# Incubation time



# Propagation time





# Time to failure

