

WG II

Size effect considerations for linear structural elements of timber

**In the frame of COST E55
'Modelling of the performance of timber structures'**

R Brandner

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**Center of Competence
for Timber Engineering and Wood
Technology**

**at Center for Structural Engineering
Graz University of Technology**

Content:

- Linkage to MoU
- **TOPIC I** – Some general thoughts – independent of the material
 - Definition
 - Types of ‘size effects’
 - ‘Sub-size effects’
- **TOPIC II** – ‘statistical length effects’
 - Theoretical examinations – independent of the material
 - Practical examinations on timber

‘Size effects’ – Linkage to MoU of COST E55:

Main objective of COST E55:

“... to provide the basic framework and knowledge required for the efficient and sustainable use of timber as a structural and building material ...”

- Every material property is general related to boundary conditions
- Especially every strength property is related to a reference size / volume
- Design of the ultimate load requires the conversion of strength values

Specific objectives of COST E55 (selected):

“... to improve the fundamental understanding of timber material and engineered timber products ...”

- Material properties of structures depend on size and loading situation

“... to assess robustness and system aspects for timber structures ...”

- ‘Size effects’ are in dependence of the system structure itself

TOPIC I:

Some general thoughts concerning ‘size effects’

- Definition
- Types of ‘size effects’
- ‘Sub-size effects’

TOPIC II:

Examinations concerning ‘statistical length effect’

- Theoretical examinations
- Practical examinations

What are 'size effects'?

'Size effects' result from **the dependency of material characteristics on the structural size.**

EVERY native and EVERY artificial material is subjected to 'size effects'

General, the interest on 'size effects' is focused on strength properties $\rightarrow \mathbf{f} \rightarrow \{\text{size} \mid \theta\}$

Types of ‘size effects’

Main ‘size effects’ and describing theories (acc. Bažant), advanced I/II:

‘Statistical size effects’:

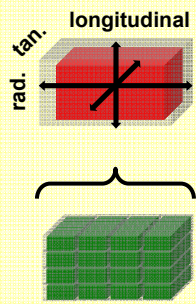
- As a result of the randomness of material characteristics
- Describable by the ‘extreme statistics theory’ → ‘weakest link theory’
acc. Weibull
- Constraints and basis of theory:
 - Perfect brittle material behaviour
 - Serial system (like a chain)
 - Equal distributed characteristic of single elements
 - Equal stressed single elements
 - Appr. of lower tail of life cycle distribution by exp. distr.

$f_{\text{RVE}} \xrightarrow{\text{iid}} f(\mathbf{X}_i | \theta)$
**Failure at the
,weakest link‘**

$$\left(\frac{f_1}{f_2} \right) = \left(\frac{V_2}{V_1} \right)^{k_V}$$

Concerning constraint 'serial system'

RVE

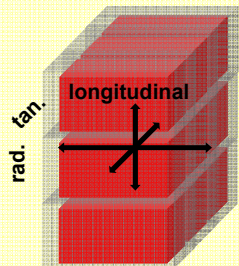


$f_{p,0,long}$ ← → $f_{p,0,long}$

$f_{p,0,long}$ ← → $f_{p,0,long}$

$f_{s,0,long}$ ← → $f_{s,0,long}$

RV



$f_{p-s,0,long}$ ← → $f_{p-s,0,long}$

Types of ‘size effects’

Main ‘size effects’ and describing theories (acc. Bažant), advanced II/II:

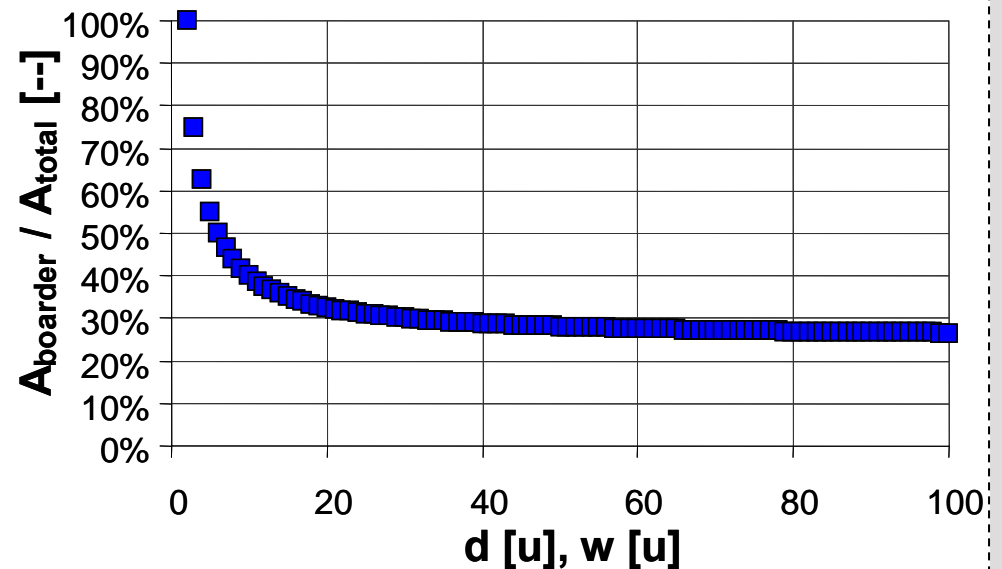
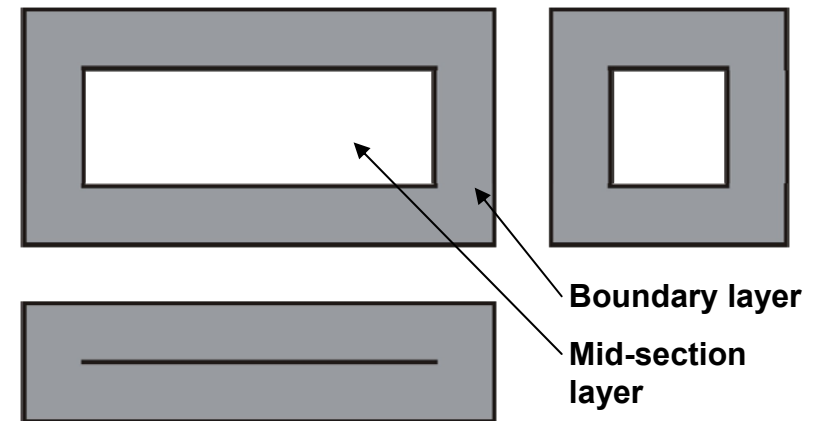
‘Energy release size effects’ / ‘fracture mechanics size effects’:

- Due to release of stored energy and redistribution of load within residual elements within a system structure after partial failures
- In case of non perfect brittle material behaviour like ‘quasi brittle materials’
- Describable by ‘fracture mechanics theory’

'Sub-size effects' acc. Bažant, advanced I/IV

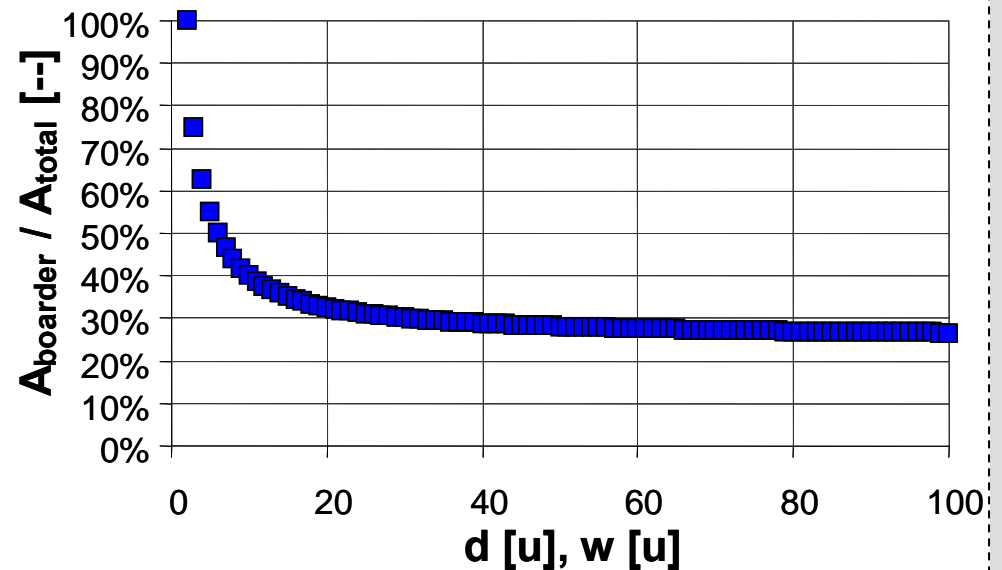
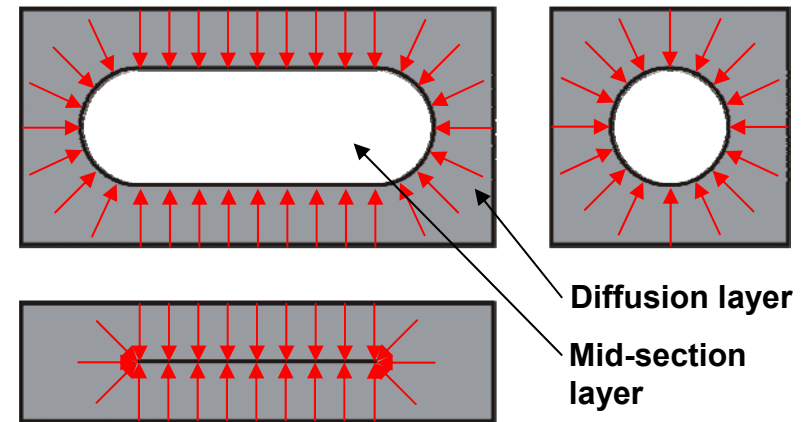
'Boundary layer effects':

- Differences in build-up between boundary- and midsection layer
 - Due to natural material build up
 - E.g. timber: cut fibers, juvenile and adult timber sections, cut knots, knot position at the edges, etc.
 - Due to production of artificial materials
 - Flaws in mid section
 - Hardening of boundaries
 - Distribution of aggregates, etc.



‘Sub-size effects’ acc. Bažant, advanced II/IV**‘Diffusion phenomena’:**

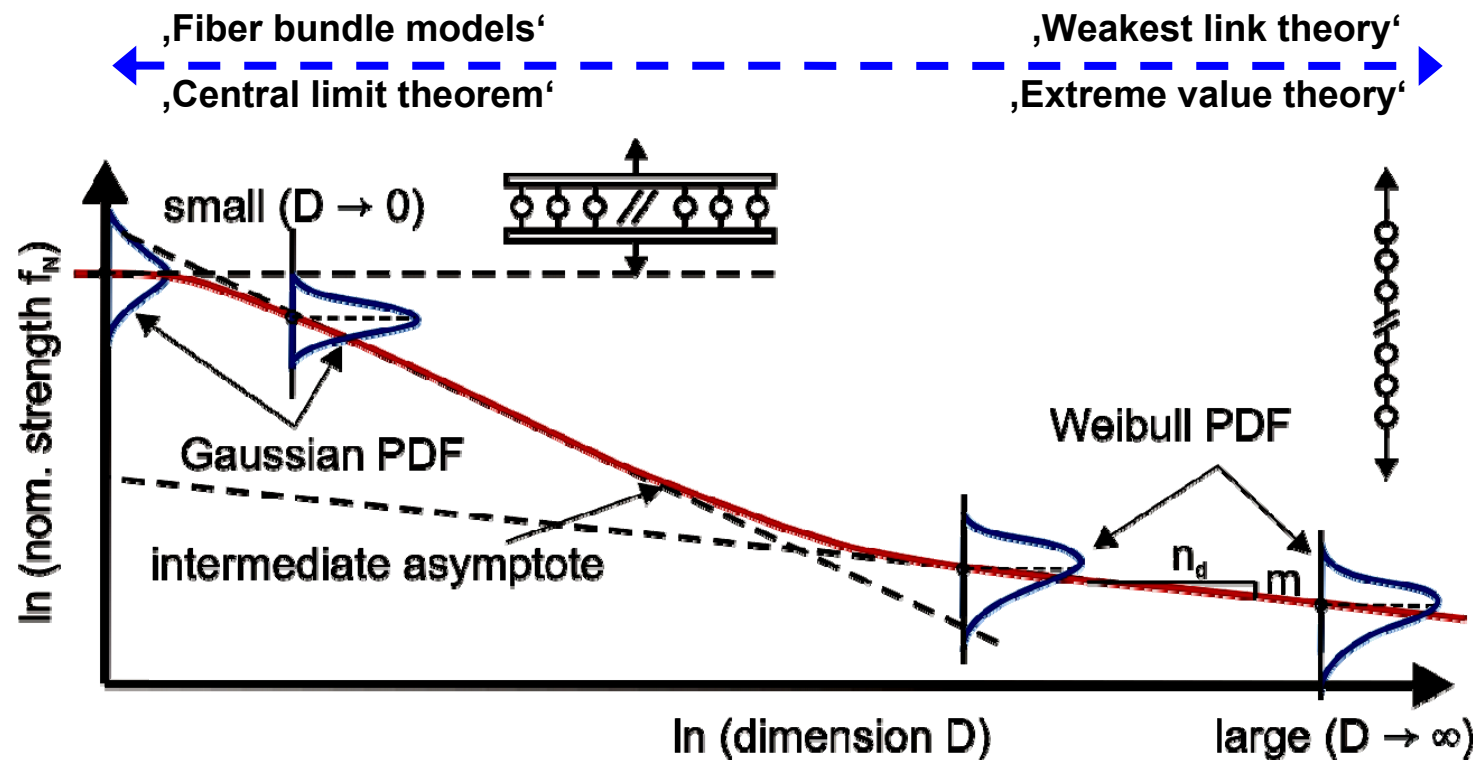
- **Delayed transport of water, temperature, other chemicals and climate effects in cyclic loading**
 - E.g. timber: orthotropic behaviour in diffusion of substances
 - Ratio of surface vers. volume → geometric effect



‘Sub-size effects’ acc. Bažant, III/IV

‘Transition of system classification’:

- System $D \rightarrow \text{DRV}$ → parallel (averaging effect)
- System $D \rightarrow \infty$ → serial



‘Sub-size effects’ acc. Galileo, IV/IV

‘Material inherent constraint’:

- Finite properties defined by the material inherent maximum capacity

‘... a small dog could probably carry on his back two or three dogs of his own size; but I believe that a horse could even not carry even one of his own size.’

(Galileo 1700’s)

- With increase of volume own weight becomes more and more important even for light-weight structures
- High failure probability if structures are loaded near their maximum capacity

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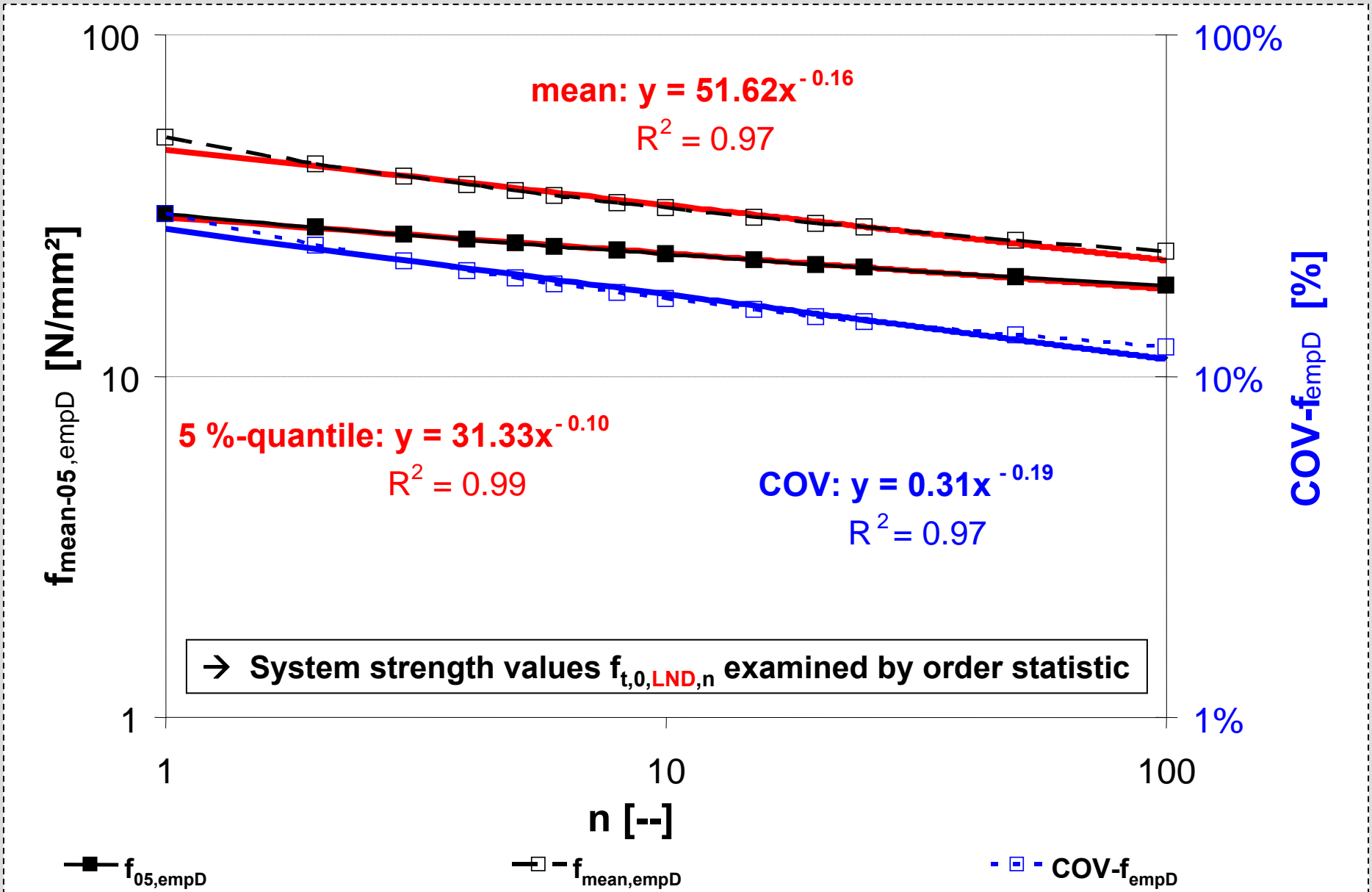
Linear timber structures – Analysis of ‘statistical size effect’:

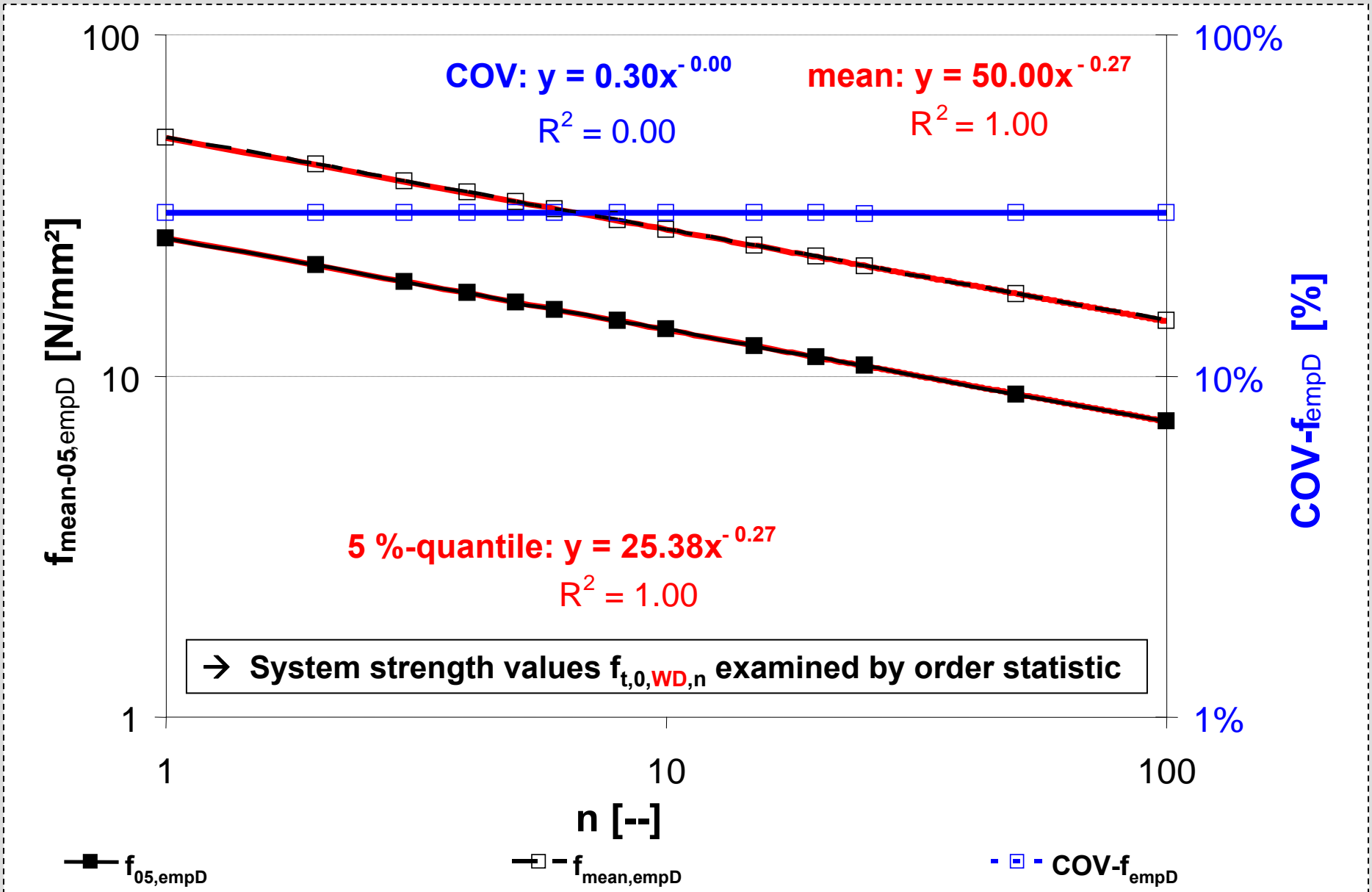
Theoretical examination:

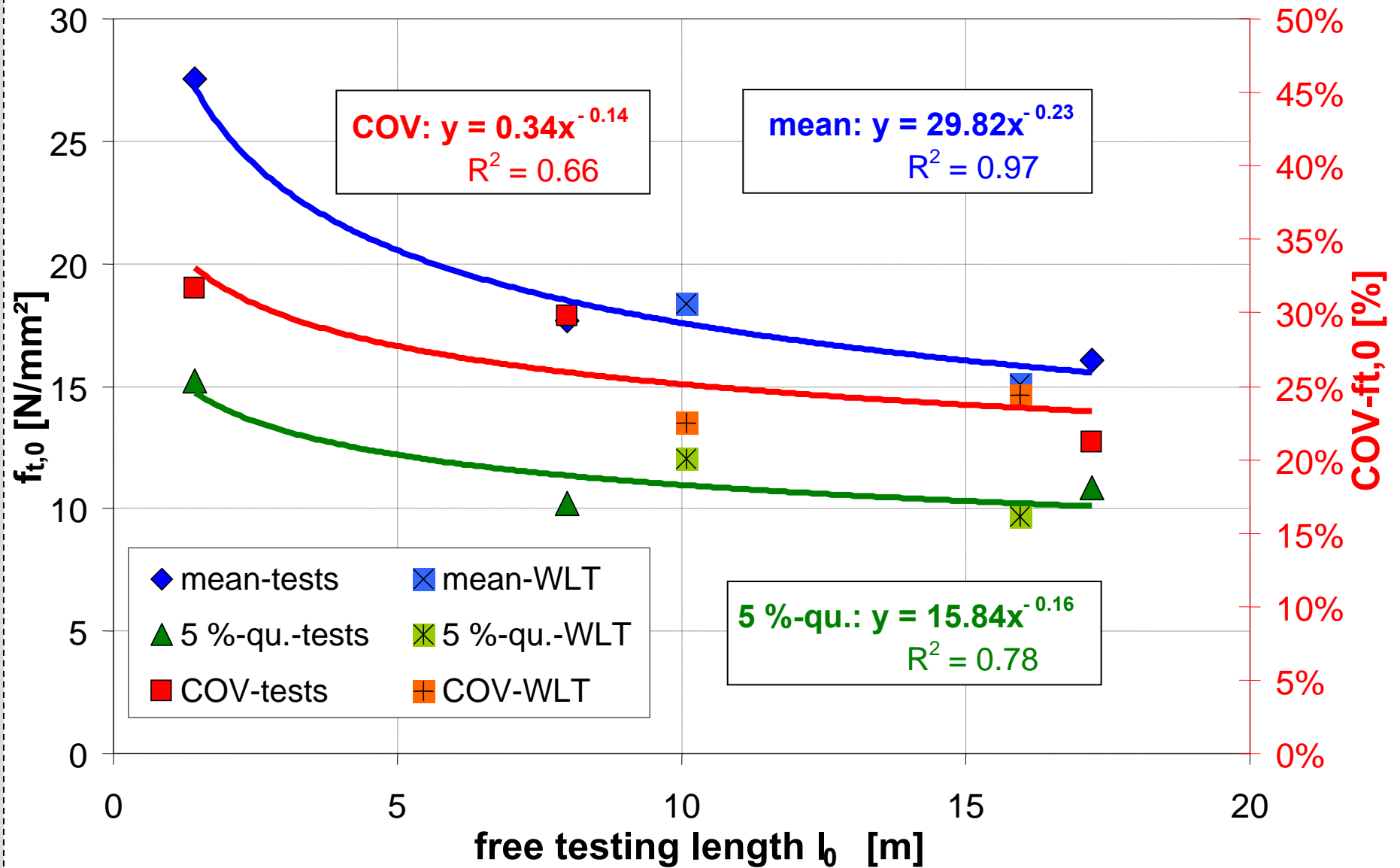
- Examined statistical distribution models:
 - WD (2-p. and 3-parametric)
 - LND (2-p. and 3-parametric)
- Application of Monte-Carlo simulations due to lack of closed solution of Integrals based on ‘extreme statistic theory – **minimum**’ – ‘weakest link theory’

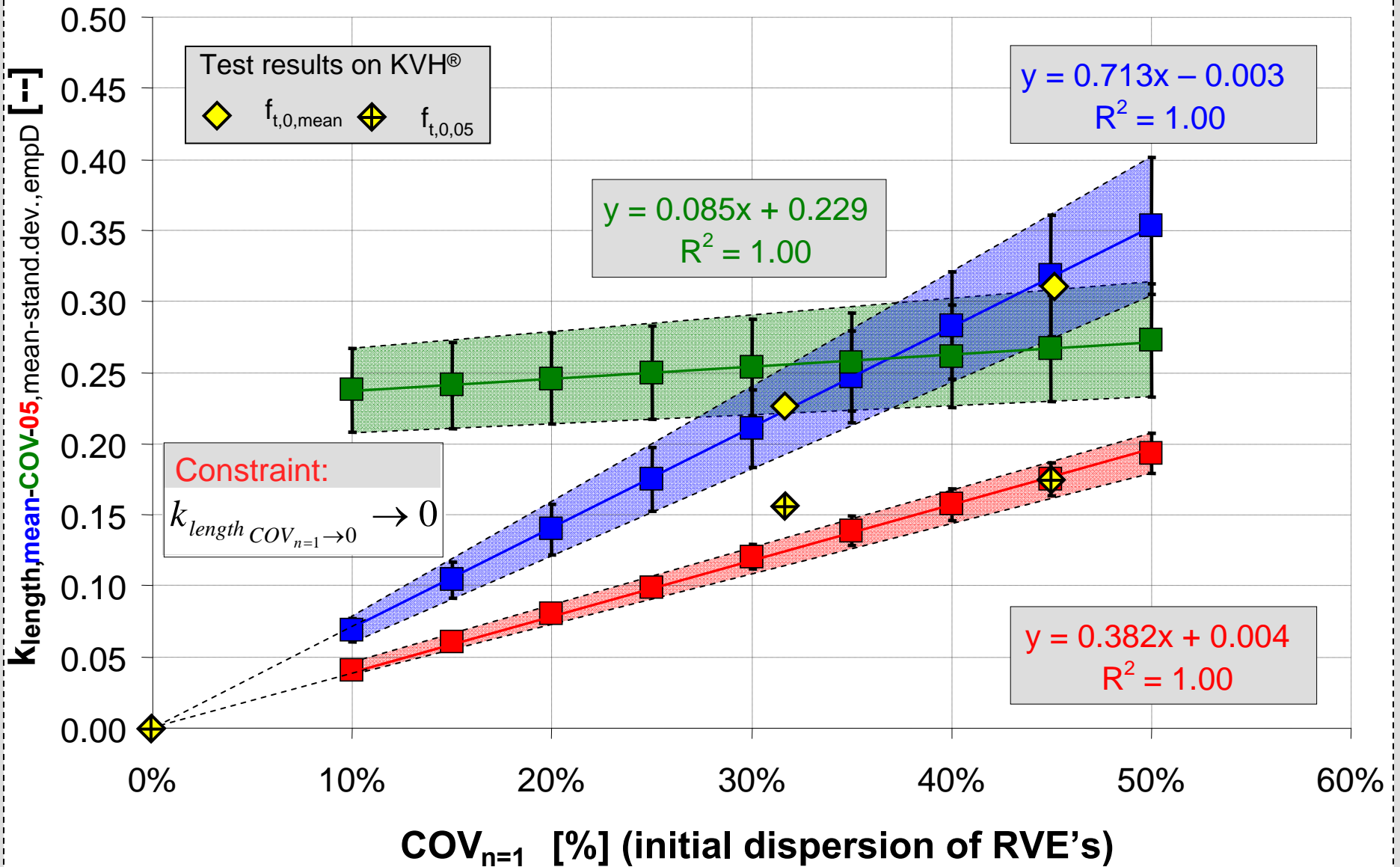
Practical examination:

- Tension tests of finger jointed construction timber (KVH®)
- Two series
 - Spruce, Middle Europe, $b / h = 200 / 60$ mm, ungraded
 - Free testing length: **2,800** mm (210 #)
 - Spruce, Middle Europe, $b / h = 160 / 60$ mm, graded S10 (acc. DIN 4074)
 - Free testing span: **1,440** mm (98 #), **7,982** mm (52 #), **17,222** mm (42 #)









Conclusion concerning the ‘statistical size effect’ on $f_{t,0,LND}$:

Modelling:

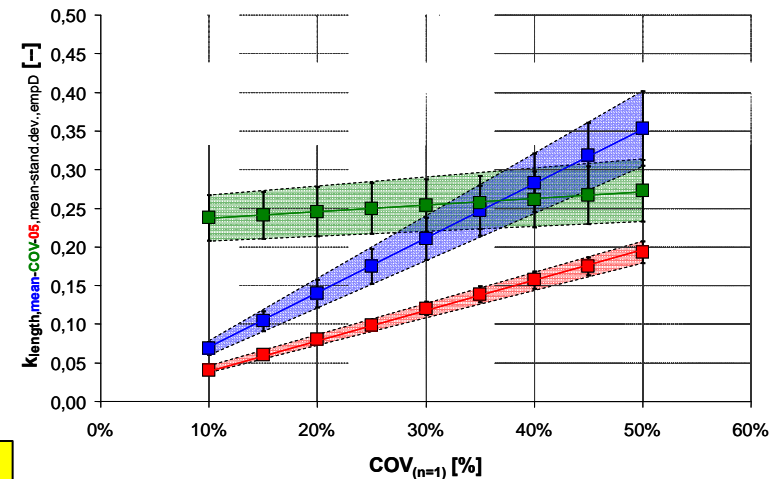
- Constraint:

$$k_{length, COV \rightarrow 0} \rightarrow 0$$

- Simplifications for RVE’s with $f_{t,0,LND}$:

$$k_{length, mean, LND} \approx 0.7 \cdot COV_{n=1}$$

$$k_{length, 05, LND} \approx 0.4 \cdot COV_{n=1} \rightarrow 0.6 \cdot k_{length, mean, LND}$$



Proposal (in regard to EN 14374 for LVL):

→ Proposal for the regulation of $k_{length,t}$ for $f_{t,0,l,05,LND}$ even for $l > l_{ref}$!!!

$$k_{length,t} = \left(\frac{l}{l_{ref}} \right)^{\alpha_t} \rightarrow \left(\frac{l}{9 \cdot w_{ref}} \right)^{\alpha_t} = \left(\frac{l}{1350} \right)^{\alpha_t}$$

$$\alpha \rightarrow f \{ DM_{n=1}, COV_{n=1} \}$$

$$\alpha_{t,LND} = 0.4 \cdot COV_{n=1}$$

Contact

DI (FH)

Reinhard Brandner

research assistant

+43 (0) 316 873-4605

reinhard.brandner@tugraz.at

Inffeldgasse 24, A-8010 Graz

DI Dr. techn.

Thomas Bogensperger

research assistant

+43 (0) 316 873-4608

bogensperger@tugraz.at

Inffeldgasse 24, A-8010 Graz

DI

Georg Jeitler

research assistant

+43 (0) 316 873-4612

georg.jeitler@tugraz.at

Inffeldgasse 24, A-8010 Graz

Univ.-Prof. DI Dr. techn.

Gerhard Schickhofer

scientific leader and head of department

+43 (0) 316 873-4600

gerhard.schickhofer@tugraz.at

Inffeldgasse 24, A-8010 Graz



Center of Competence
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at Center for Structural Engineering
Graz University of Technology