

**COST E55** – Eindhoven, October 2007

# **Shear failure in glulam frames**

## **An actual case**

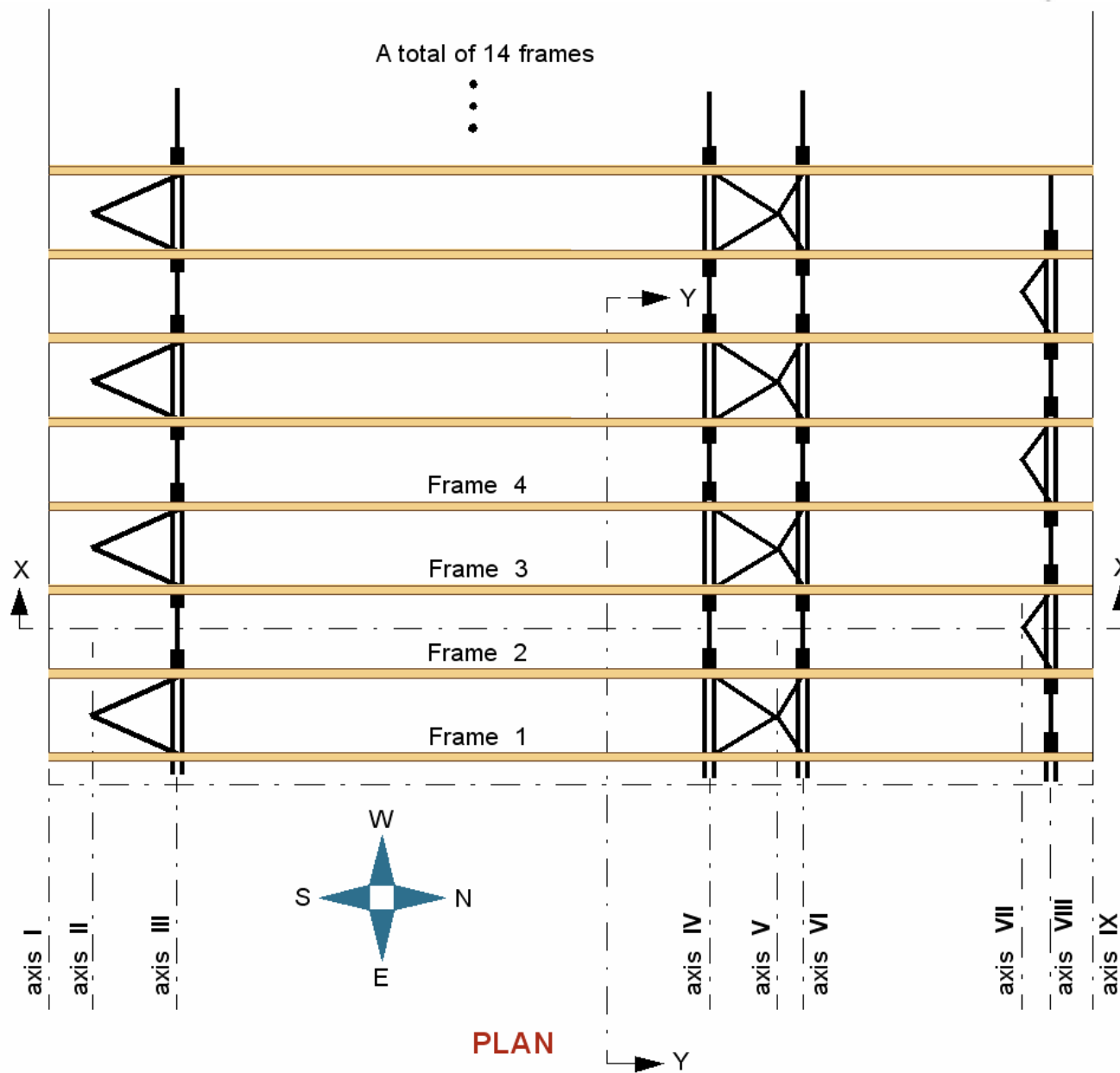
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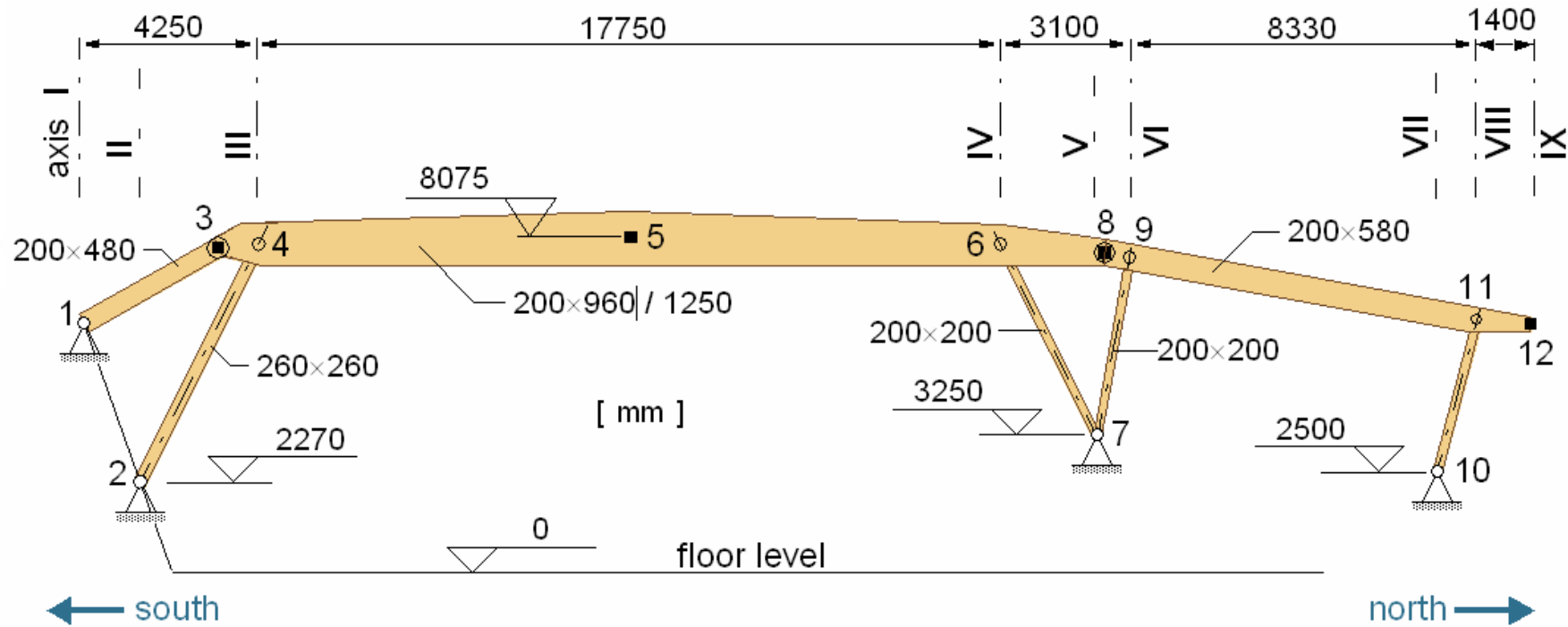
# The structure

sports centre built in 2001

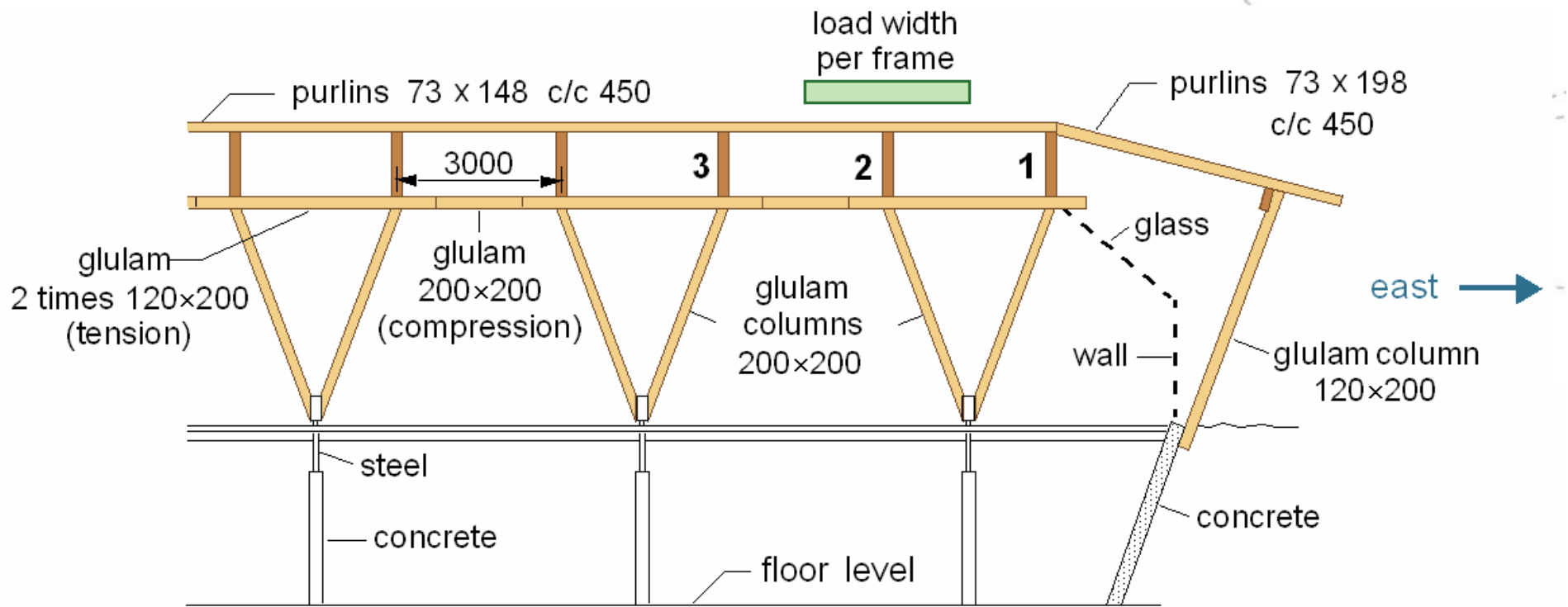




a typical frame



**SECTION X - X**



## SECTION Y - Y



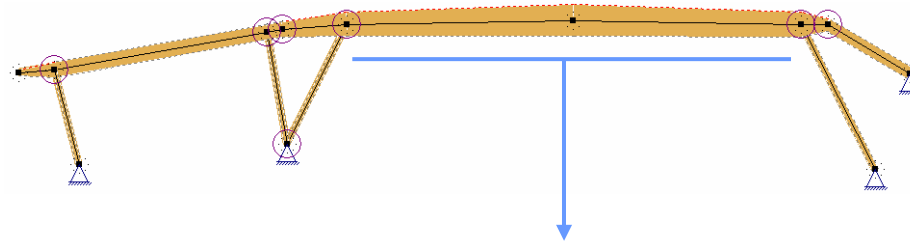


# The problem

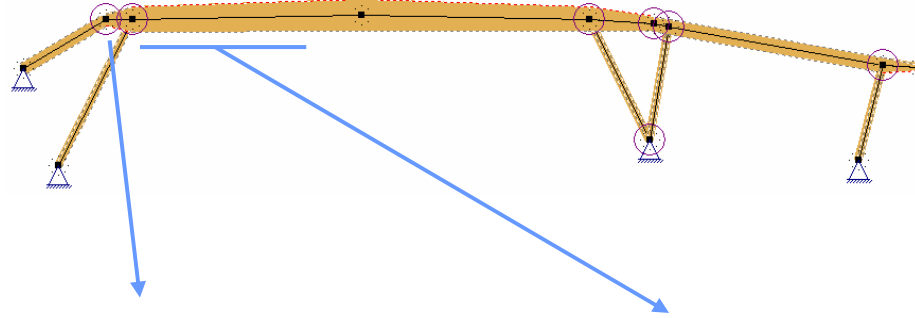
- At about 8 pm on March 20, 2005, the players of an ongoing indoor bandy training session heard high cracking noise from the ceiling.
- The caretaker was notified and the hall was evacuated.
- In one beam (frame 2) a long crack was visible from the floor.
- On closer inspection severe shear cracks were found in the main beam of 3 frames – number 1, 2 and 10.
- The snow loading was measured the following day; it was found to be from 2,3 to 3,5 kN/m<sup>2</sup>, well below the design load of 5,5 kN/m<sup>2</sup>



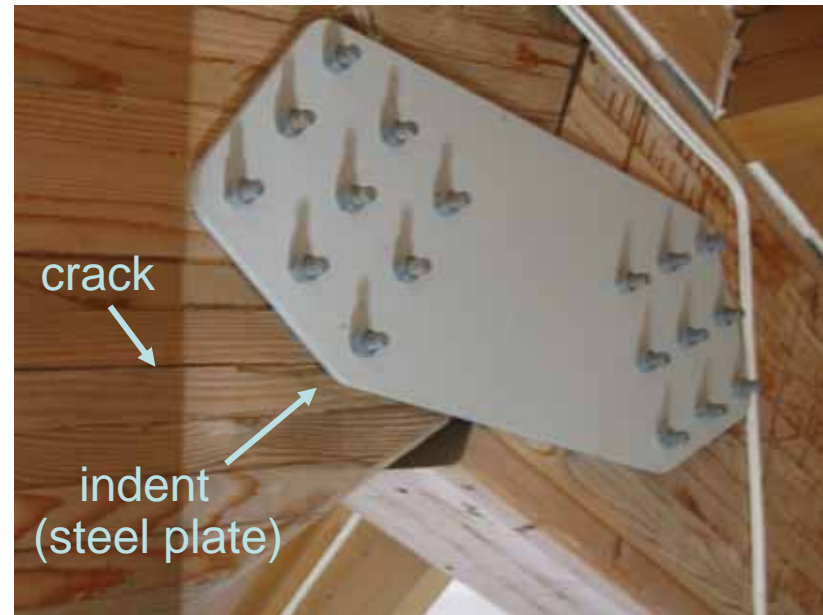
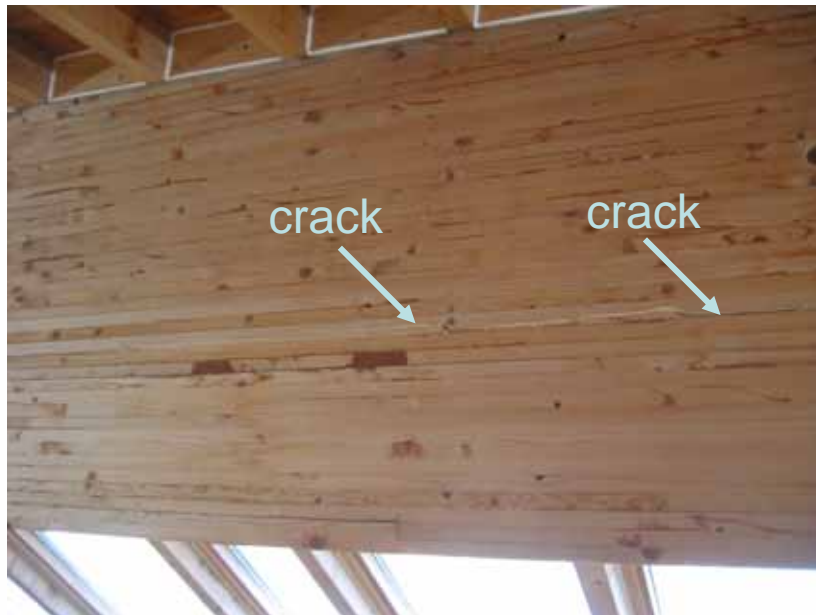
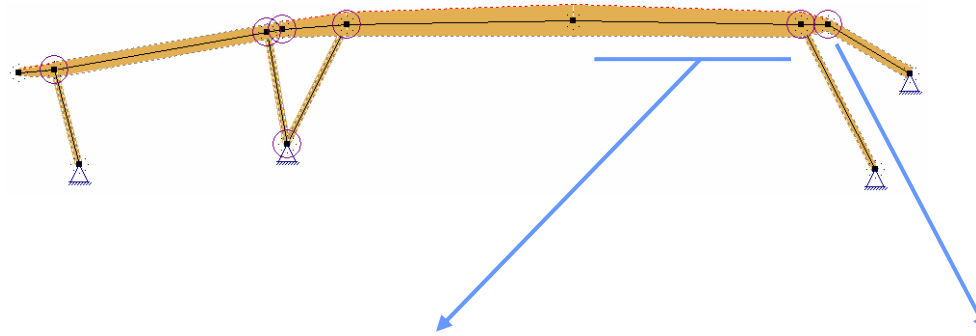
## Frame 2



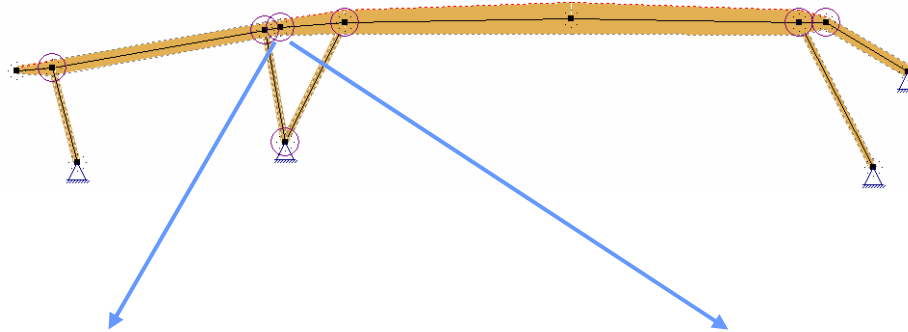
## Frame 2



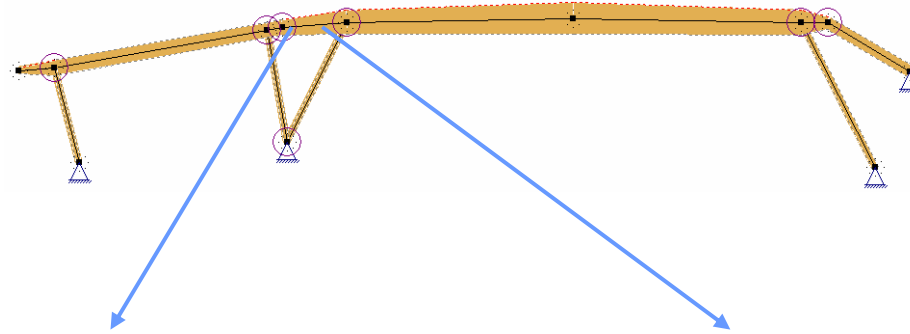
Frame 1



# Frame 1



# Frame 1



## Maximum (measured) vertical displacements [ mm ]

<b>Frame</b>	03.03.05	16.03.05	08.04.05
<b>1</b>	195	199	190
<b>2</b>	190	188	168
<b>3</b>	106	88	76
<b>10</b>		103	

↑  
no snow

# The cause ?

- Possible candidates:
  - excessive loading ? - hardly, but loading uncertain
  - incorrect design ? - not likely, but cannot be ruled out
  - poor detailing ? - ? (joint rotation)
  - moisture (shrinking/swelling) ? - not likely
  - glulam quality ? - variable, so yes, a possible culprit

# Loading

Design load, including form and load factors

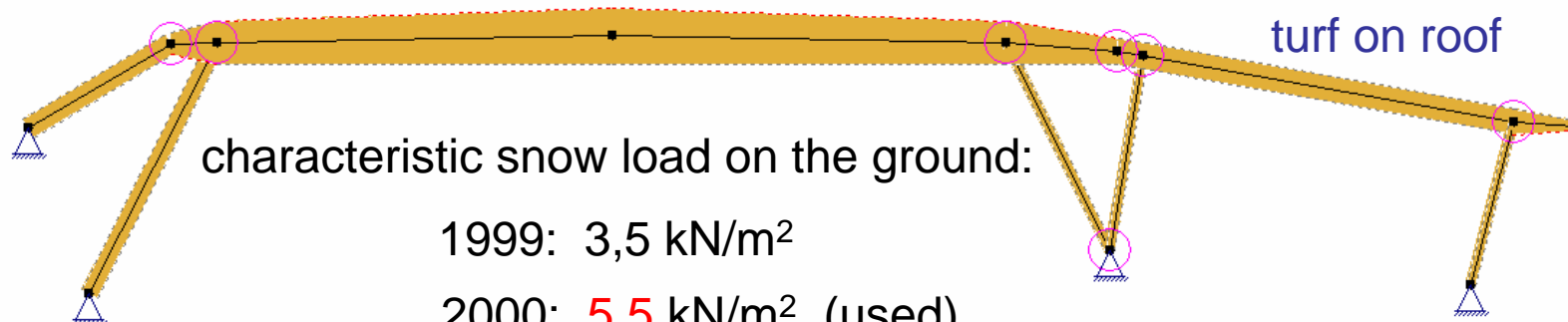
Actual (measured) load at time of failure

snow $s$ [kN/m]	$s_1 = 23,1$	$s_3 = 19,8$	$s_1 = 9,15$	$s_3 = 6,9$
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index 1 → frame 1

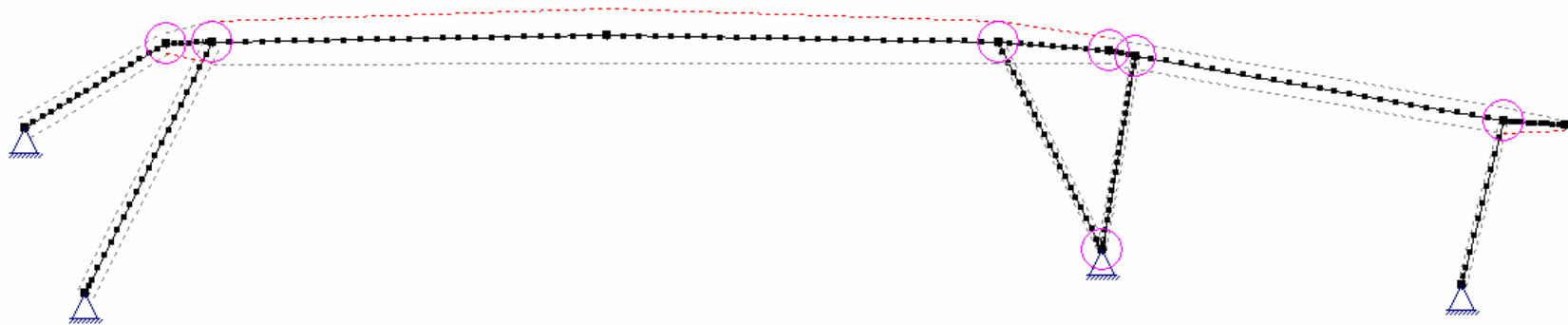
index 3 → frame 3

dead load $g$ [kN/m]	$g_1 = 10,5$	$g_3 = 9,0$	$g_1 = 8,75$	$g_3 = 7,5$
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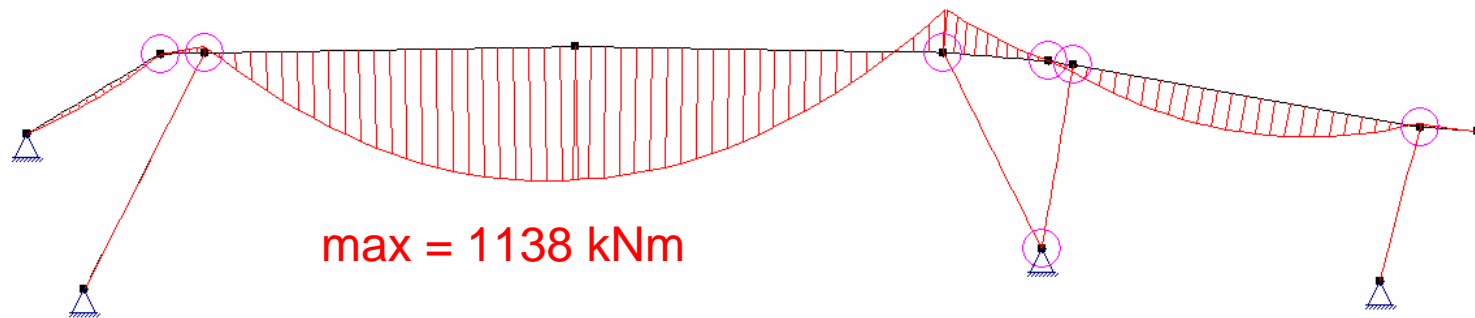
## Some calculations



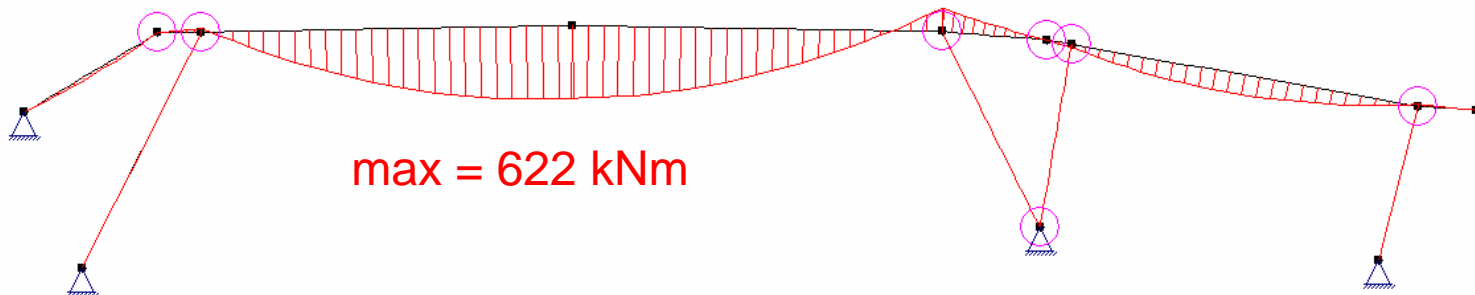
computational model – 2D frame analysis

# Bending moment – Frame 1

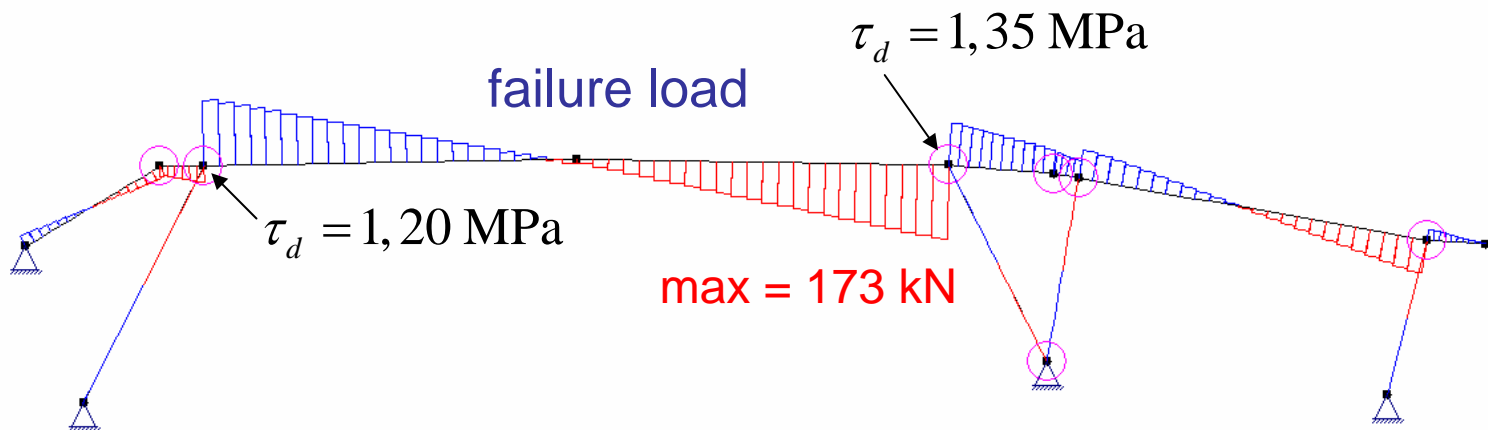
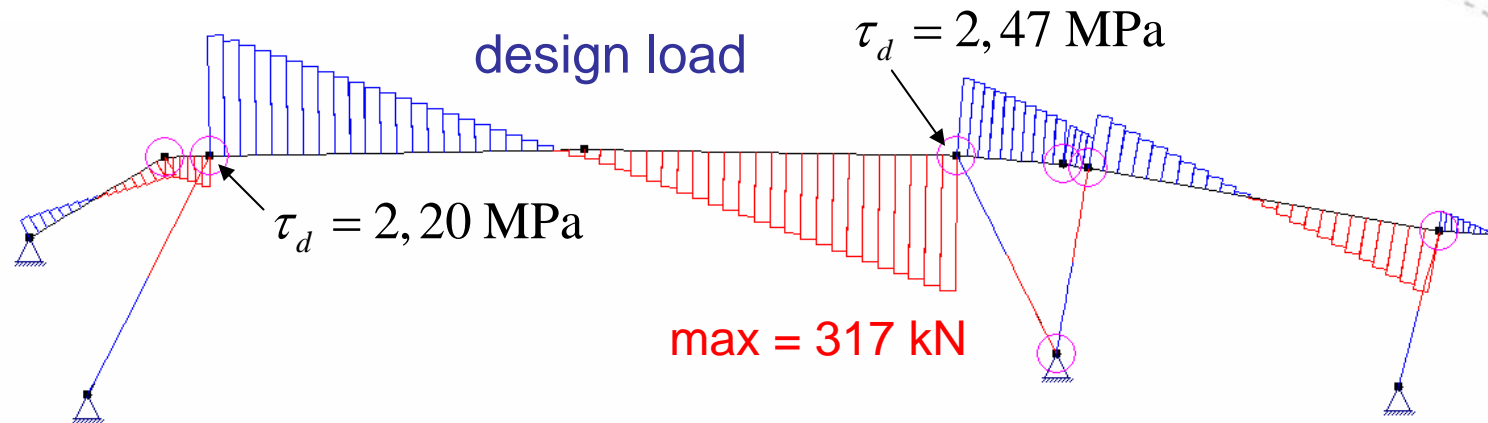
design load



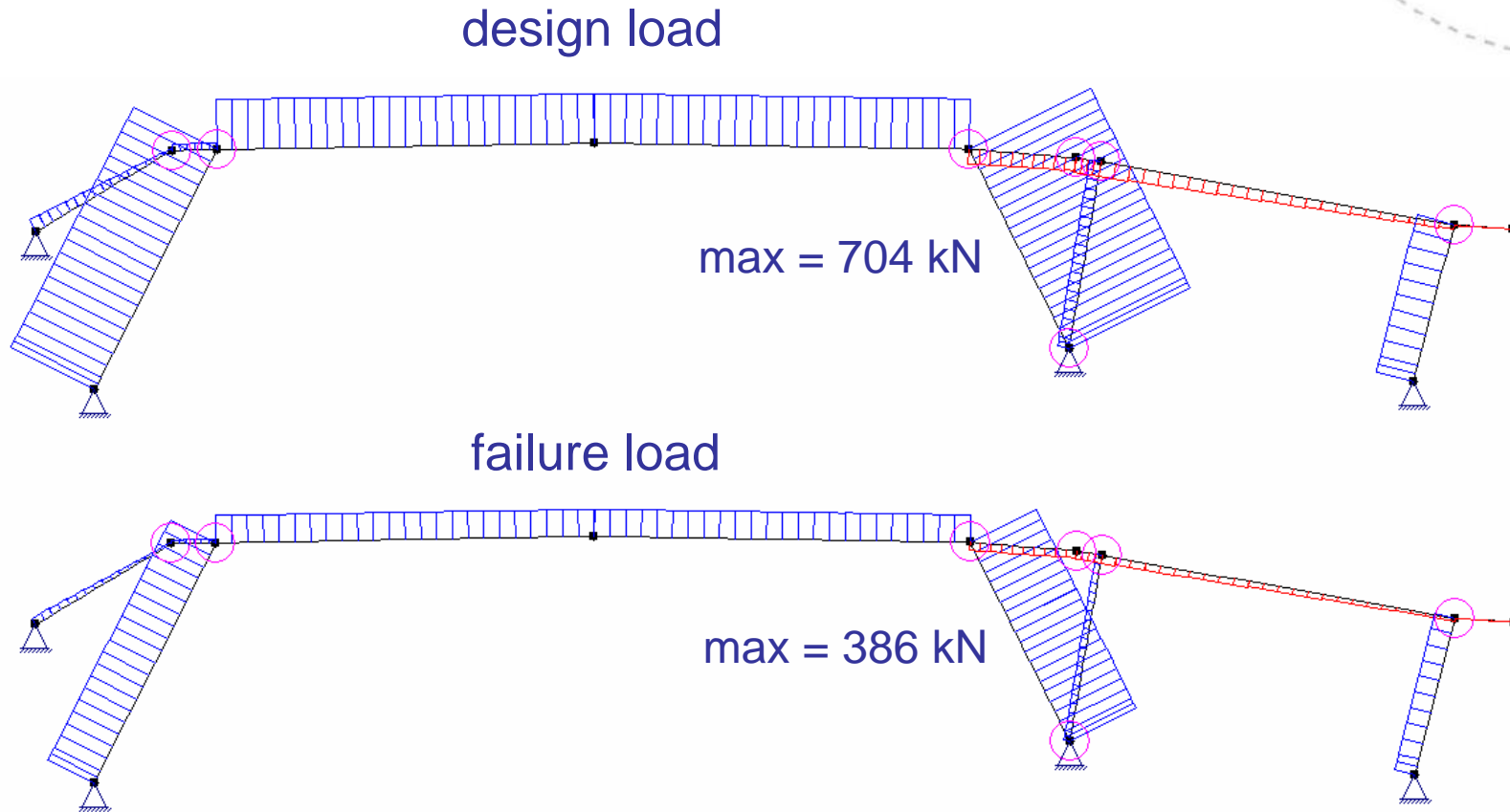
failure load



# Shear force – Frame 1

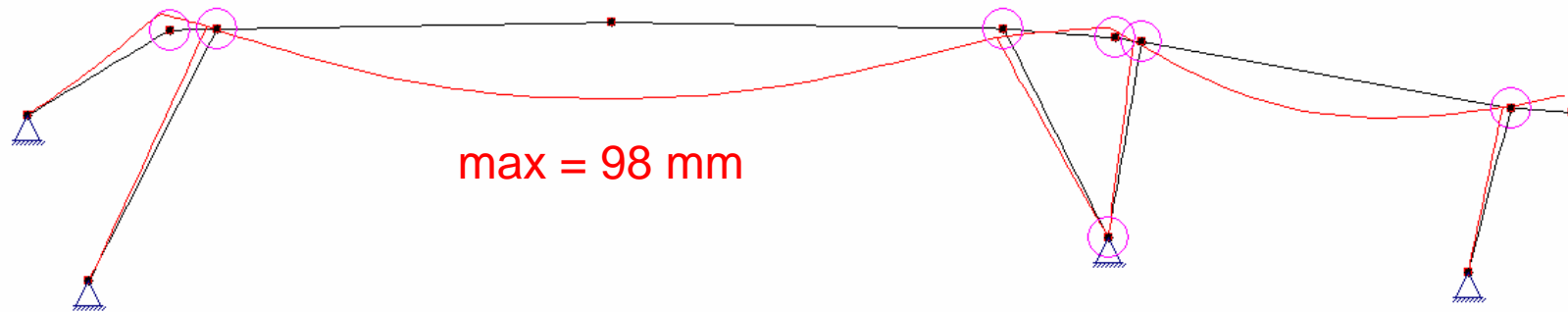


# Axial force – Frame 1



# Displacements – Frame 1

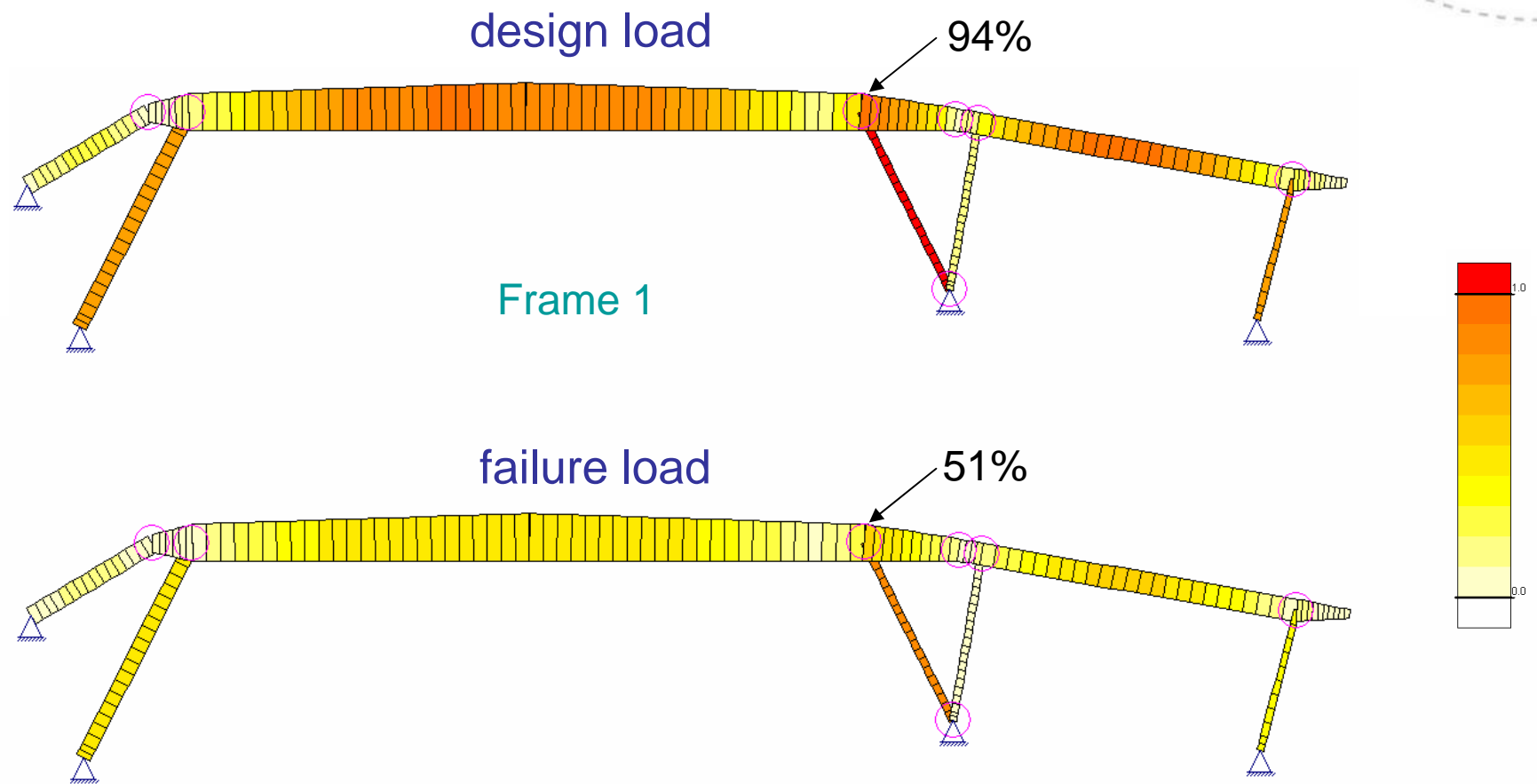
design load



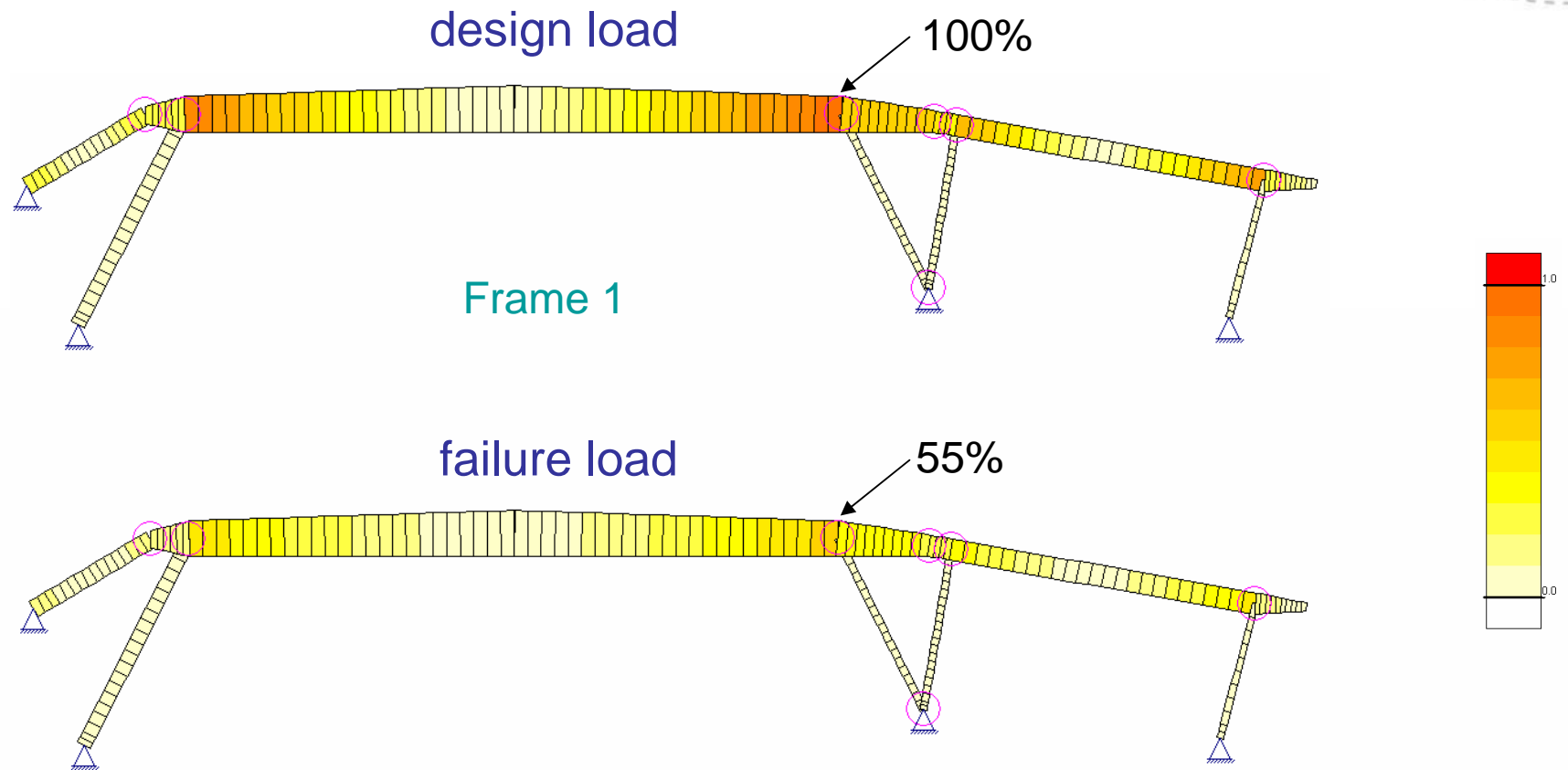
failure load



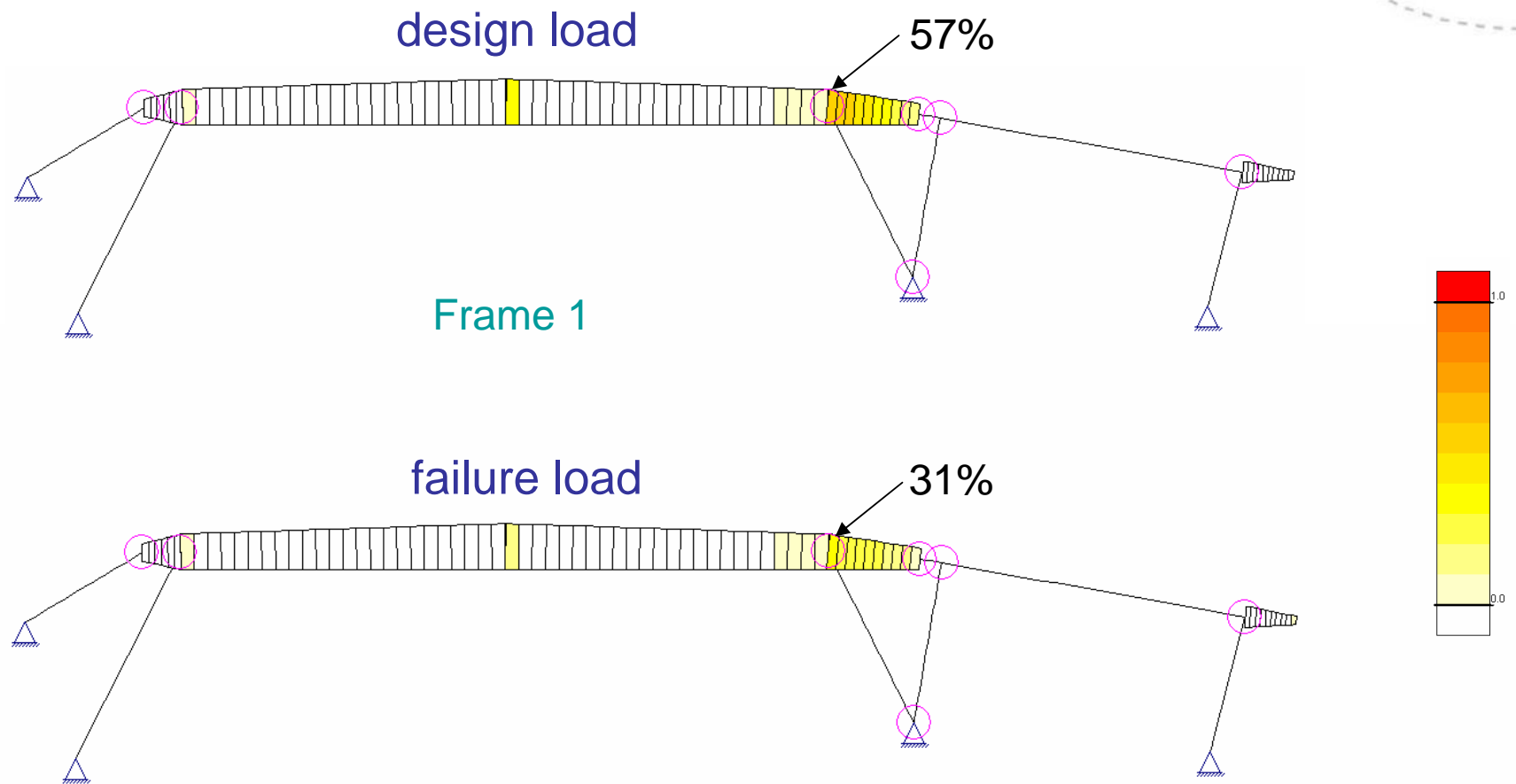
# Capacity – NS 3470 combined bending and axial force



# Capacity – NS 3470 shear

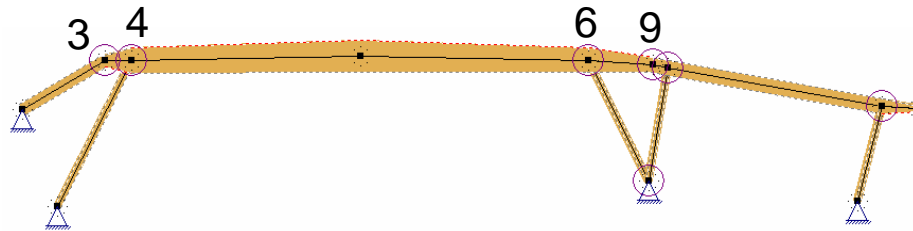


# Capacity – NS 3470 tension perpendicular to grain



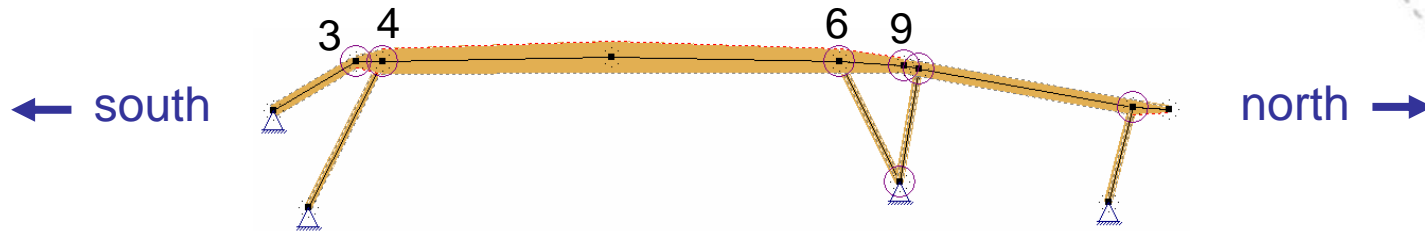


## Most likely failure scenario



1. Failure starts in a defect glue line (21) at point 4 of frame 2 and the crack propagates towards the middle of the beam.
2. The shear stresses at the faulty (3rd) glue line of frame 2 increases and causes a complete collapse of this glue line (from 4 to 6).
3. The resulting sagging of frame 2 increases slightly the loading on frame 1 and this causes a shear failure to start in a defect glue line at node 4 – the shear crack propagates towards the middle of the beam.
4. The additional sagging of frame 1 causes a large rotation at joint 9 which in turn causes a crack due to tension perpendicular to grain – this crack propagates towards, but not beyond point 6.

## Additional comments

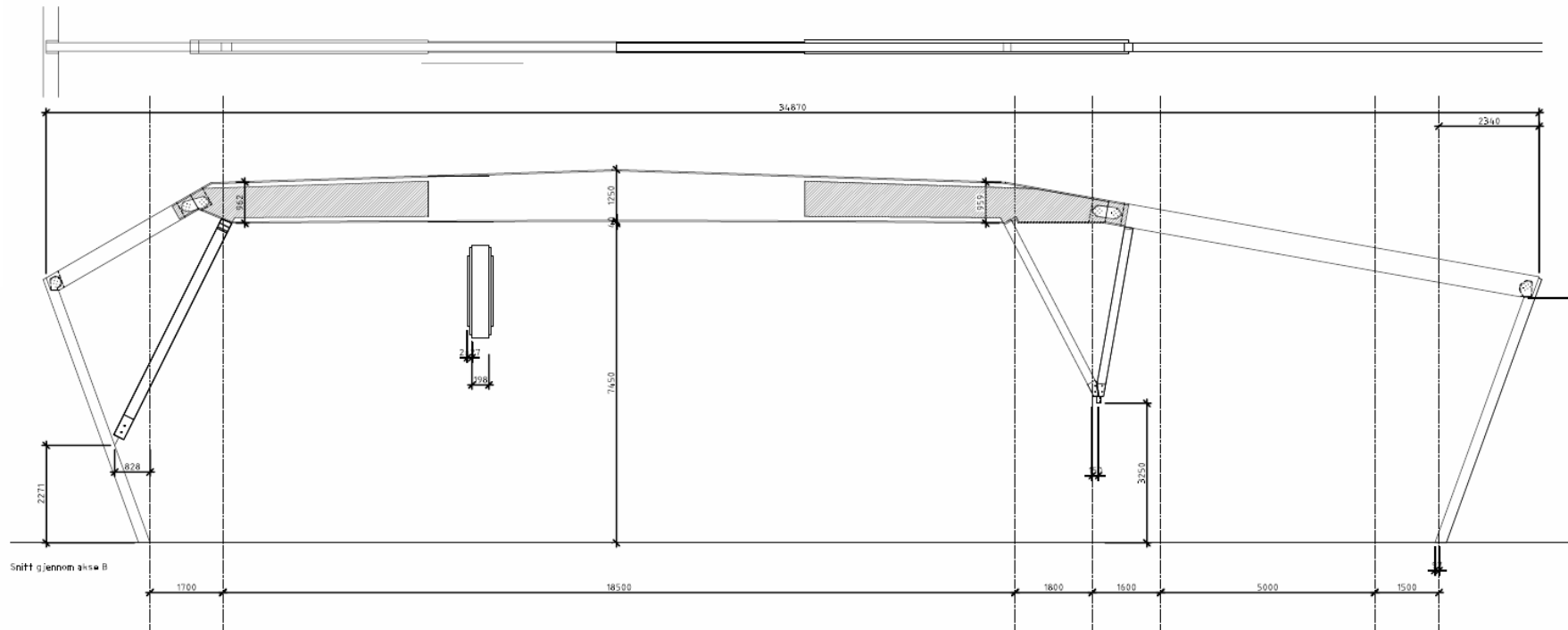


1. The sequence of events can be argued, but we are fairly confident that the failure started in the south end of the main beam.
2. The very noticeable cracking in frame 1, at and near the connection in 9, is a secondary failure (caused by a large rotation of the joint). There is only a minor crack in this region of frame 2 and none at all in frame 10.
3. The (computationally) highest shear stresses are just to the left of point 6, but there are no visible cracks in this part, in any frame .
4. Initially we suspected the connection at point 3 to be part of the problem, but the crack in this area is *below* the connection in frame 1, *above* the connection in frame 2 and in the *middle* of the connection in frame 10.
5. Weight of gravel and turf probably somewhat higher than stipulated.

# The repair

- All open cracks filled with glue and closed in correct position (beams jacked up to “normal” displacement)
- Three extra column supports for frame 1
- The three damaged frames reinforced by 27 mm Kerto Q plates glued to both sides of the entire face of the main beam + an additional layer of 45 mm Kerto Q in the most (shear) stressed areas at the ends.  
A two-component epoxy adhesive with long curing time was used.
- All (11) remaining (and not visibly damaged) beams reinforced by one layer of 45 mm Kerto Q glued to each side of the beams in the most (shear) stressed areas at the ends.

## Reinforcement by Kerto





# Thank you