

Moisture-induced stresses perpendicular to grain in cross-sections of timber members exposed to different climates

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Background

- In variable humidity conditions wood absorbs or desorbs moisture from the air. Unless the change in humidity is very slow, this will develop moisture gradients in the wood sections. These gradients will develop stresses: moisture-induced stresses.
- The present paper investigates the main parameters affecting such moisture-induced stresses, including the type of climate, the size of the timber cross-section, and the type of protective coating.
- An attempt to identify moisture- induced stresses in different European climate regions was made.



Factors affecting the moisture induced stresses

- Initial moisture content
- Type of exposure
- Size of the member
- Coatings



Moisture induced mechanical effects: Classes 1, 2, 3, 4

Classification

Conclusions from previous research

- 1. <u>Restrained shrinkage is a problem in</u> joint design and detailing
- 2. <u>Fast drying is a problem in areas</u> with surface peak perp stresses (holes, notches)
- 3. <u>Long wetting</u> is a problem where wood is under tension perp load (tapered beams)
- 4. <u>Longitudinal stresses</u>, continuous humidity cycles more important than single moisture changes.

- Moisture induced stresses is primary reason of failure
- Number of cycles or duration of load not important
- Stress analysis shows similar stress fields in successive cycles
- Strength is reduced in high humidities and still more reduced in cyclic humidities, duration of load is important



1. Restrained shrinkage



Figure 115-1. Arched column with steel parts (in white).



Figure 115-2. Crack at column fitting to the steel part.



Figure 94-1: Support connection of glulam beam to concrete column.



2. Fast drying



Fig. 9. Longitudinal through crack in glulam roof girder due to shrinkage effects. Hot water piping in the vicinity of the girder contributed to fast drying. Source: Ref. [7].



Figure 20. Cracks in pitched cambered roof beams due to restrained shrinkage. Views of both sides of a beam. Source: Ref. [7].



3. Long Wetting





Fig. 8. Crack propagation in gradient specimens, RH 40 to 80%, tested at day 5







Bsk: Cold semi-arid climate (Madrid, Salamanca, Albacete)

Csa: Warm Mediterranean climate (Lisbon, Cagliari, Palermo, Athens) Csb: Temperate Mediterranean climate (Potenza, Marsilia, Coruna, Porto) Cfa: Warm oceanic//humid subtropical climate (Zagreb, Brescia, Torino, Bologna, Roma, Foggia.) Cfb: Temperate oceanic climate (Stuttgart, Zurich, Paris, London) Dfa: Warm / humid continental climate (Kosice, Odessa, Zaporozhe) Dfb: Temperate//humid continental climate (Moscow, Warsaw, Helsinki) Dfc: Cool continental climate/subarctic climate (Rovaniemi, Lulea, Tampere) ET: Tundra climate (Chambery,

Zurich, Sofia)



Abbrev-	Type of climatic region	Example of cities within		
iation		the climatic region		
Bsk	Cold semi-arid climate	Madrid, Salamanca,		
		Albacete		
Csa	Warm mediterranean	Lisbon, Florence, Cagliari,		
	climate	Palermo, Athens		
Csb	Temperate mediterranean	Potenza, Marsilia, Coruna,		
	climate	Porto		
Cfa	Warm oceanic//humid	Zagreb, Brescia, Torino,		
	subtropical climate	Bologna, Roma, Foggia		
Cfb	Temperate oceanic climate	Stuttgart, Paris, London		
Dfa	Warm/humid continental	Kosice, Odessa, Zaporozhe		
	climate			
Dfb	Temperate//humid	Moscow, Warsaw, Helsinki		
	continental climate			
Dfc	Cool continental climate/	Rovaniemi, Lulea,		
	subarctic climate	Tampere		
ET	Tundra climate	Chambery, Zürich, Sofia		

 Table 1: Köppen-Geiger climate type classification of Europe [11].



$$G = \frac{u_{surf} - u_{\Delta L}}{\Delta L} \left[m^{-1} \right]$$

UNCOATED SECTION				
Climatic area	City	$\Delta L = 4 \text{ mm}$	$\Delta L = 10 \text{ mm}$	$\Delta L = 30 \text{ mm}$
BSK	Madrid	-5.723	-3.962	-1.379
CSA	Lisbon	-6.028	-3.955	-1.635
CSA	Florence	-7.666	-3.657	-1.514
CSB	Potenza	-5.244	-3.159	-1.264
CFA	Zagreb	-6.744	-4.584	-1.545
CFB	Stuttgart	-8.115	-4.349	-1.880
DFA	Kosice	-6.917	-5.079	-1.606
	Moscow	-6.381	-3.942	-1.954
DFB	Warsaw	-7.959	-4.584	-1.980
	Helsinki	-9.575	-5.111	-1.789
DEC	Rovaniemi	-11.83	-5.982	-2.279
DFC	Tampere	-11.23	-6.176	-2.593
ET	Chambery	-11.83	-3.592	-1.402

Table 3: 10-year analysis: Gradients of moisture content for different climatic regions at different depths for uncoated cross-section sizes (highest negative gradient values given which result in surface tension stresses).



Rovaniemi



Warsaw



Lisbon



























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Summary

- The moisture-induced stresses perpendicular to grain depend on the moisture content distribution over the cross-section and, hence, on
 the type of exposure, the size, initial moisture content, coatings.
- For timber members exposed to outdoor conditions with timber sheltered from rain, the most influencing quantities were found to be the type of climate, and the presence of a protecting coating.
- Climates characterized by larger yearly variations of relative humidity induce higher stresses, northern European climates were found to result in higher moisture gradients and thus in higher moisture induced stresses when compared with southern European climates.
- Natural variations of relative humidity were found in several cases to induce stresses perpendicular to the grain exceeding the tensile and compressive strength perpendicular to the grain.
- The presence of a protective coating is an effective measure to reduce moisture variations and, therefore, moisture-induced stresses and the consequent cracking.



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Possible reasons for the rather high calculated internal stresses

- the use of a Fickian diffusion model,
- the omission of hysteresis effects of sorption,
- and possibly higher actual mechano-sorptive properties perpendicular to grain than predicted