



André Carlen, La Conversion/LIGNUM

# On the consideration of moisture induced stresses in timber structural design

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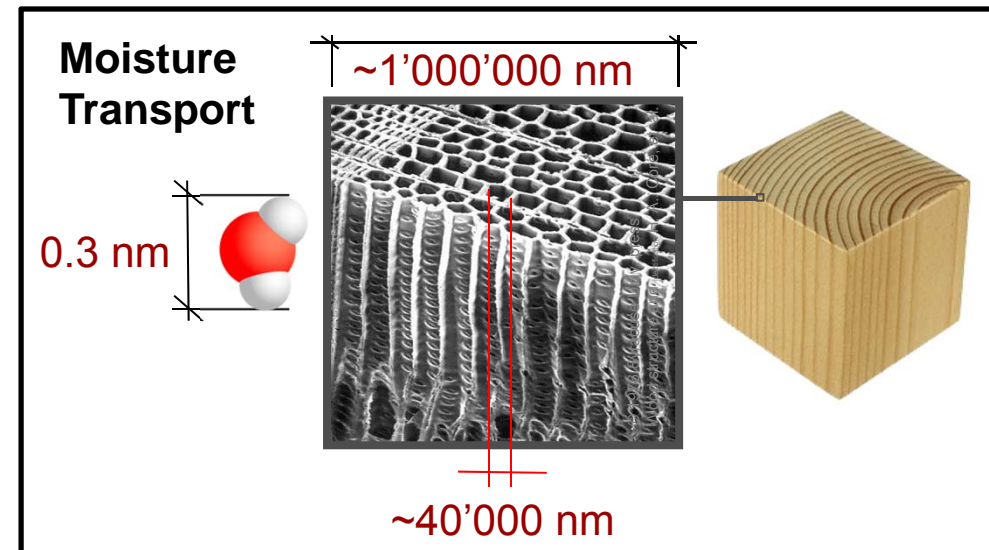
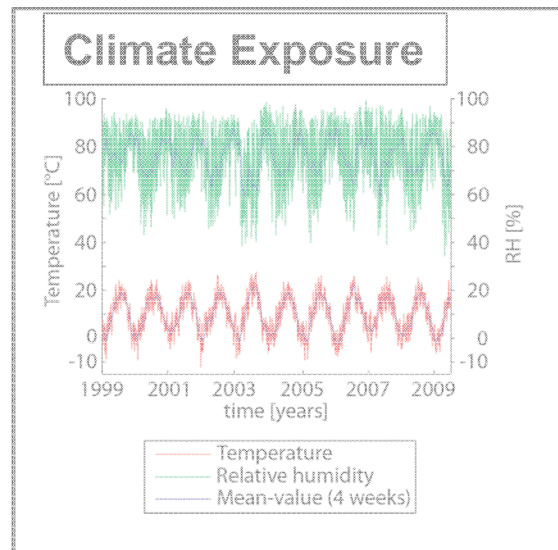
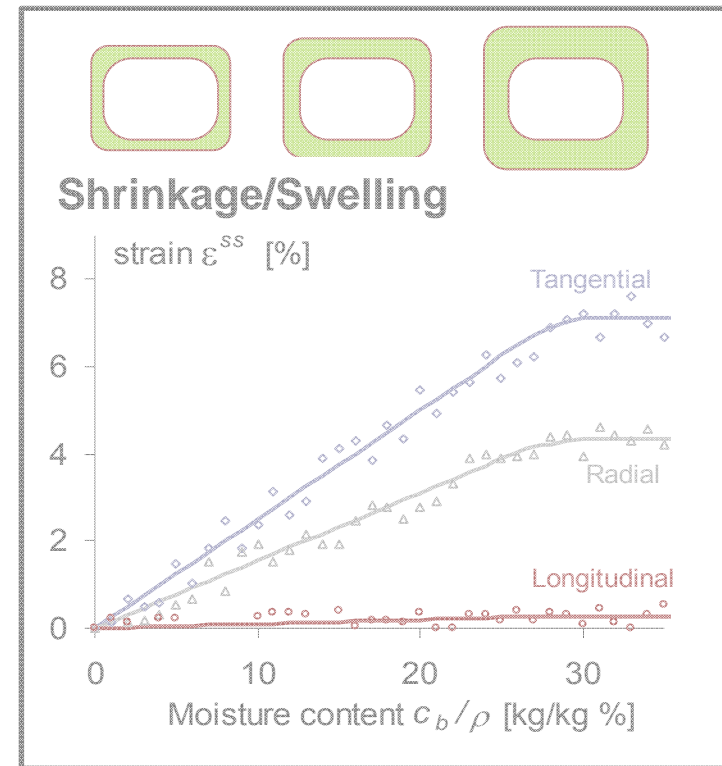
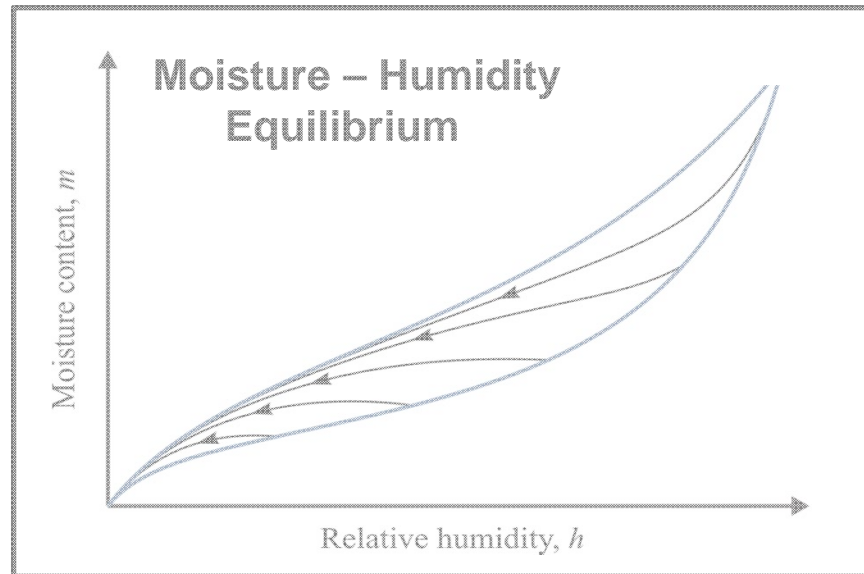
COST E55, Final Conference  
Zurich, May 2011



# Overview

- Problem setting
- Design codes, present
- Analysis of failures and malfunctions
- Moisture induced stresses, explicit
- Implications and outlook

# Problem setting



# Design codes, present

e.g.



$$r_d = k_{\text{mod}} \frac{r_k}{\gamma_m}$$

$k_{\text{mod}} = 1$  : Climate and loading conditions similar to standard test conditions

$k_{\text{mod}} \neq 1$  : Climate and loading conditions depart from standard test conditions  
→ Choice depending on 3 x 3 climate and load classes.

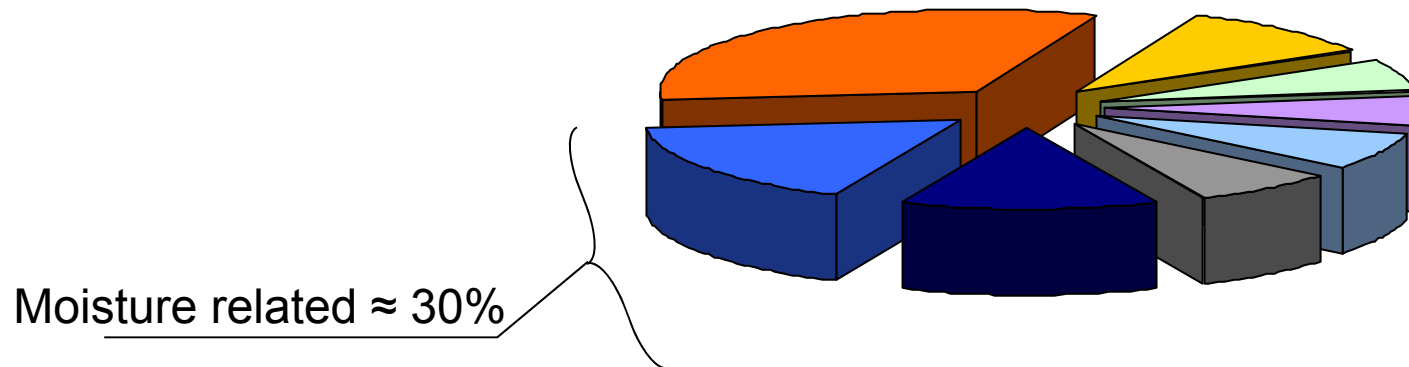
- Load duration classes, the 'shortest' in the combination is relevant
- Climate classes only with direct criteria for absolute surrounding RH

# Analysis of failures and malfunctions

## COST E55 WG 1:

Conclusion from national surveys\* on timber structure failures:

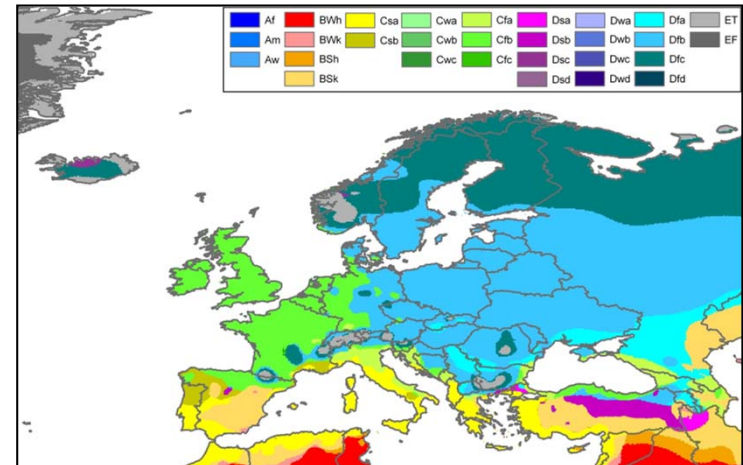
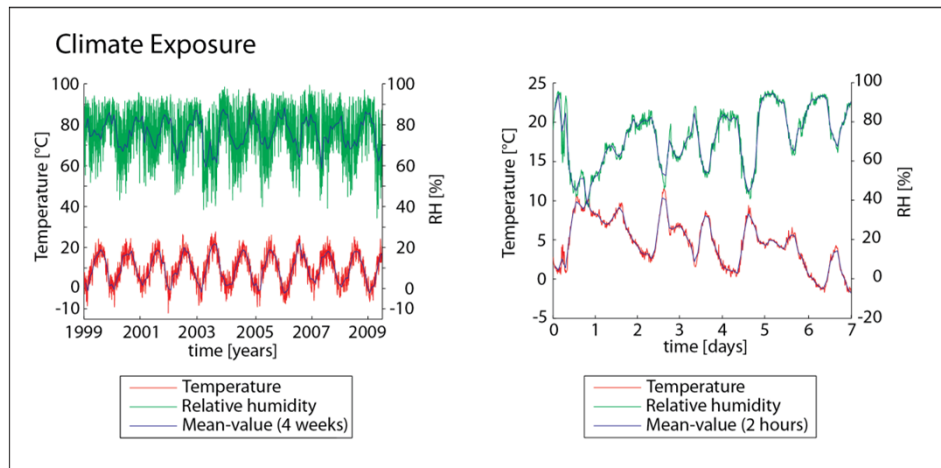
A significant part of the failures assessed were a (indirect) result of humidity and variation of humidity.



Finland, Germany, Slovenia & Sweden

# Moisture induced stresses, explicit

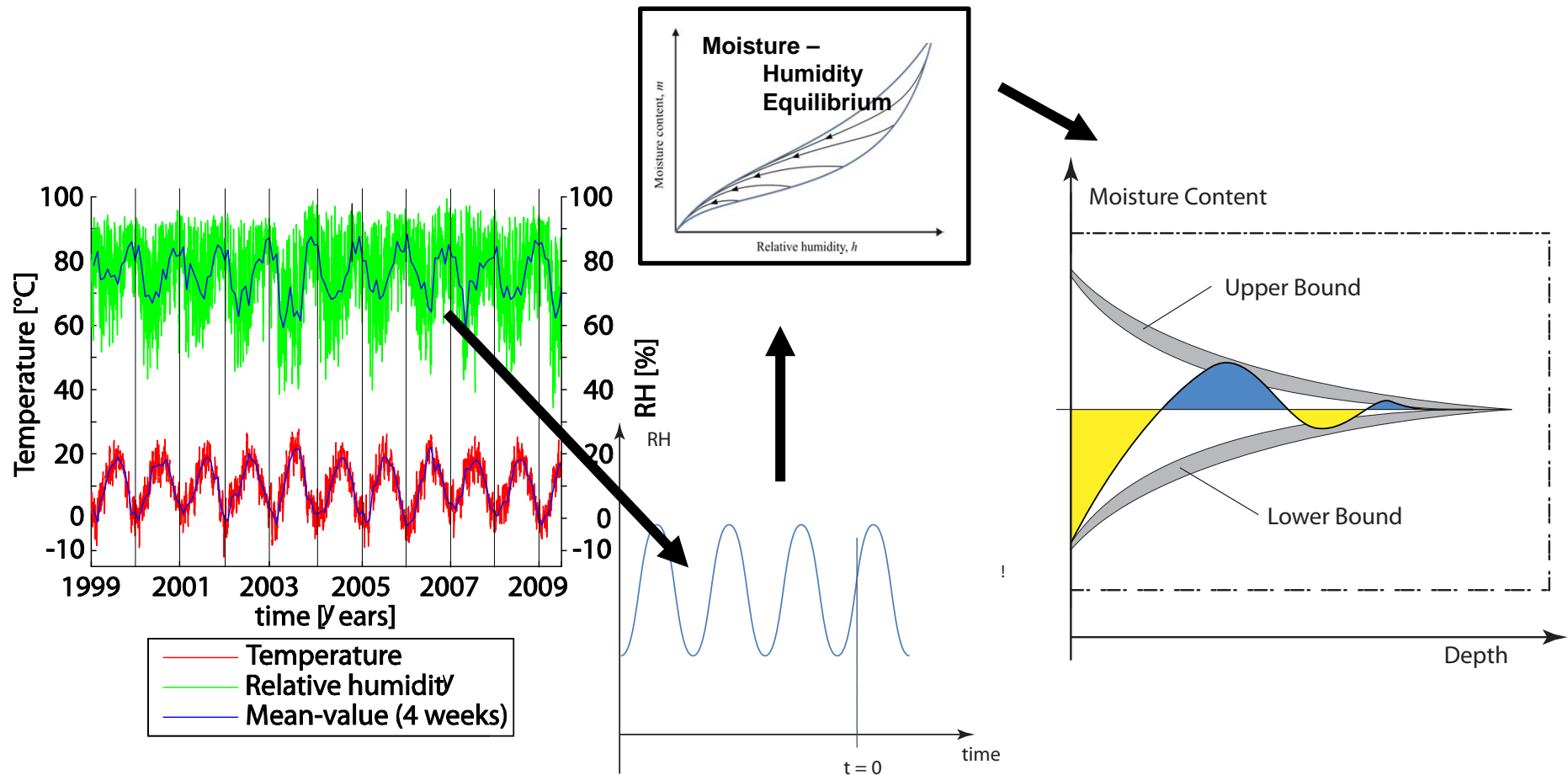
## 1. Climate exposure:



- Relevant period dependent on scale / treatment of components
- Extremes are relevant
- Combination with other external loads (correlation)

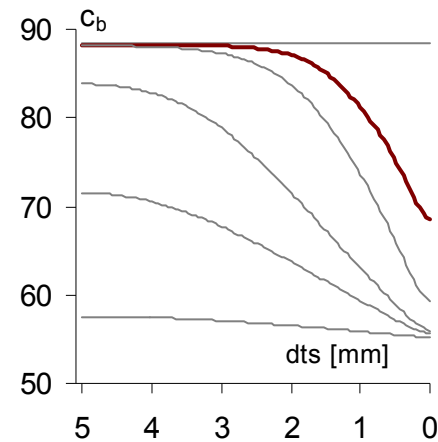
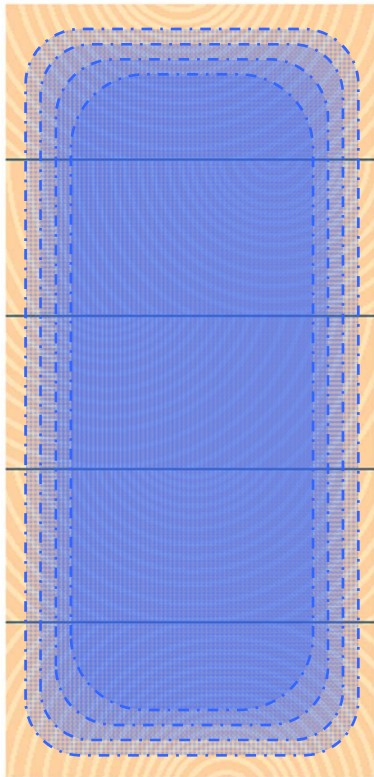
# Moisture induced stresses, explicit

## 2. Moisture transport / sorption:

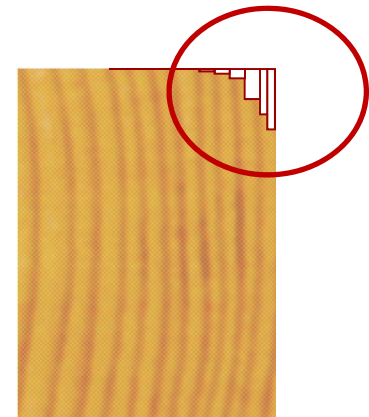


# Moisture induced stresses, explicit

## 3. Constraint strain and stress:



Hypothetical  
free shrinkage



# Moisture induced stresses, explicit

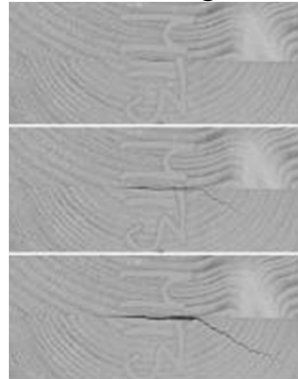
## 4. Localised fracture:

Drying



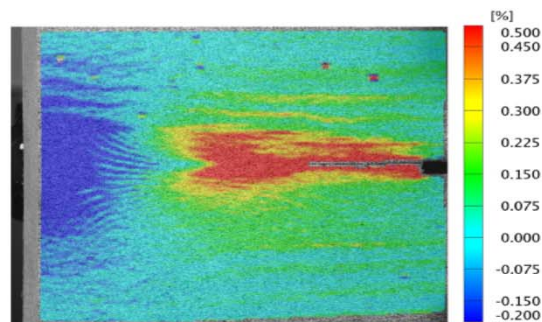
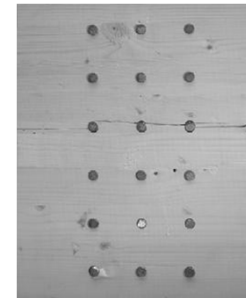
Toratti

Wetting

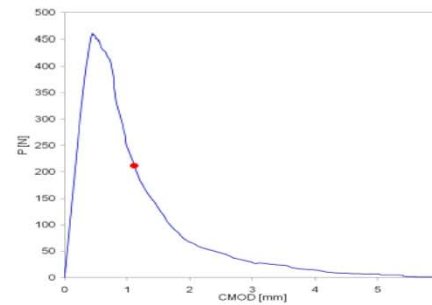


Jönsson & Thelandesson

Connections



(k) Transverse strain,  $\epsilon_y$



(l) Load: 211 N ; time: 254 s

# Moisture induced stresses, explicit

## 5. Design situation and scale issue:

Design situation A:  
No external load

Criteria:       no cracks,  
                    serviceability

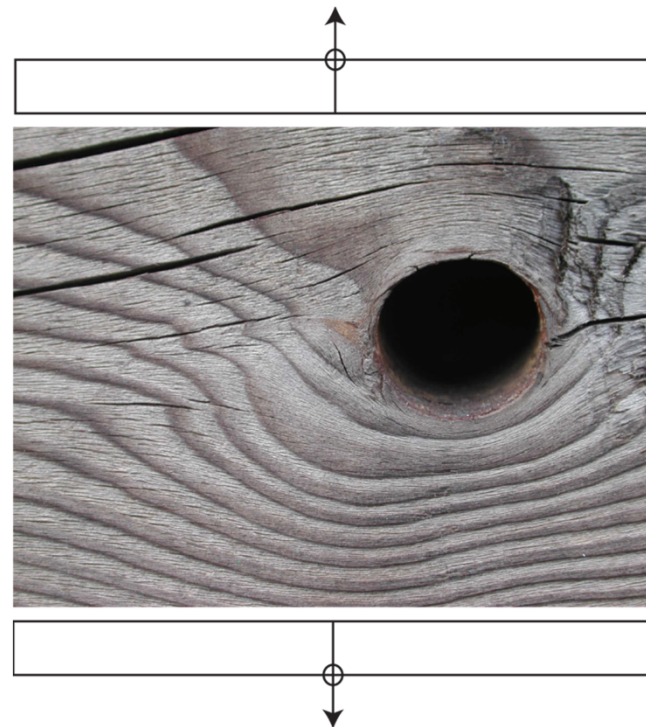


# Moisture induced stresses, explicit

## 5. Design situation and scale issue:

Design situation B:  
Load perp. to the main  
grain direction

Criteria:        no failure,  
                      ultimate



Superposition of external load effects with estimations of MIS

# Moisture induced stresses, explicit

## 5. Design situation and scale issue:

## Design situation C: Load effects in main grain direction

Criteria: no failure,  
ultimate



Superposition of external load effects with estimations of MIS not possible

# Moisture induced stresses, explicit

## 5. Design situation and scale issue:

Design situation D:  
Load effects in main  
grain direction

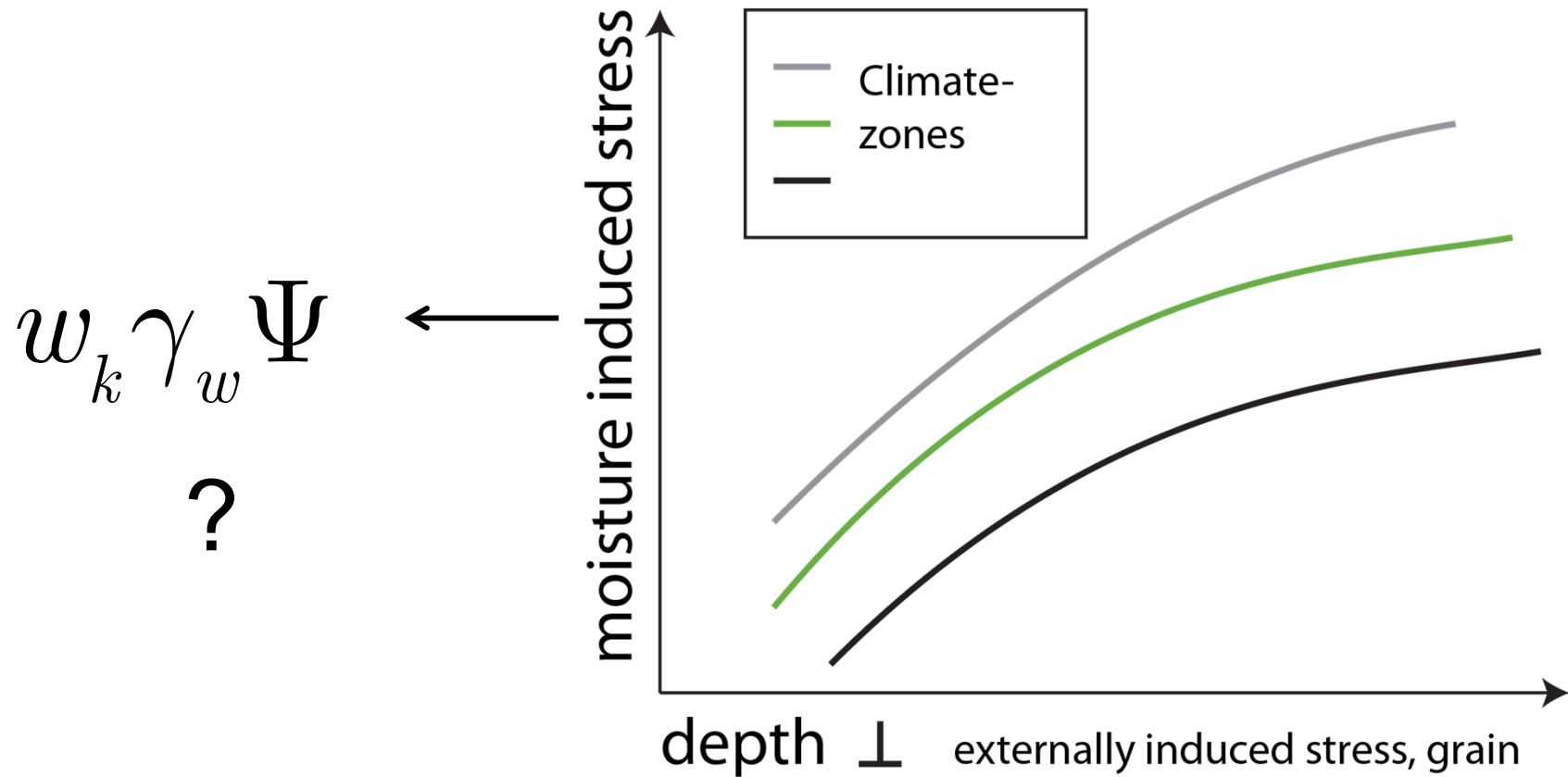
Criteria:            no failure,  
                              ultimate



Superposition of external load effects with estimations of MIS  
not possible

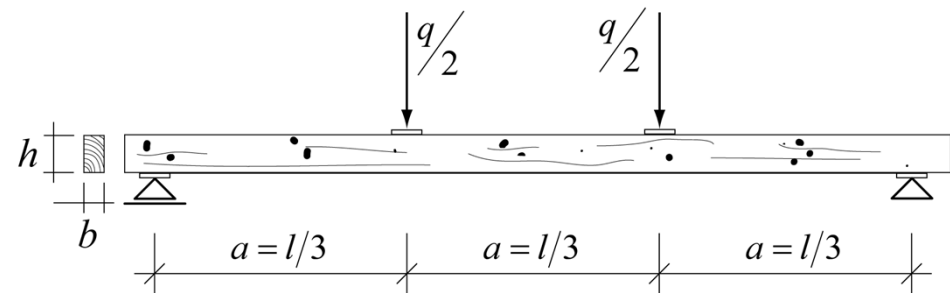
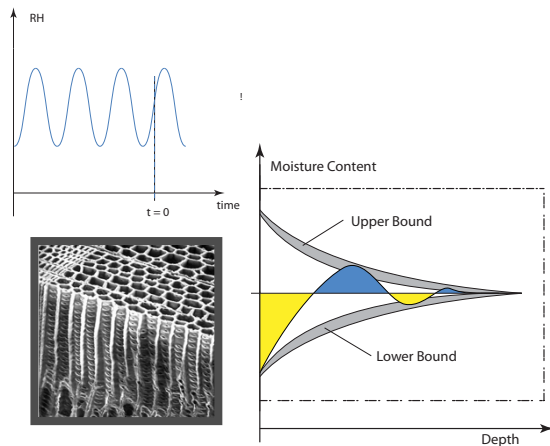
# Implications and outlook

When superposition is possible:



# Implications and outlook

When superposition is not possible:



$$s = \frac{ql}{bh^2}$$

How do we come over the scale issue ?

After a tension test

Thank you  
for your attantion !

